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GRAPHICAL TRAJECTORY COMPENDIUM OF CALIBER .50 AND 20 mm PROJECTILES IN AN AIR TO GROUND AND GROUND TO GROUND ROLE

October 1973

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Munitions Development & Engineering Directorate

U.S. ARMY ARMAMENT COMMAND FRANKFORD ARSENAL PHILADELPHIA, PENNSYLVANIA 19137

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This report is a compendium of trajectories in air to ground and ground to ground role of projectiles shapes of possible interest in cannon caliber ammunition applications. The 20MM projectiles shapes are M53, M56 and SAPI. The caliber 50 drag curves are the M2 and M8.

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INTRODUCTION

The data compiled in this report provides engineering information needed in making evaluations of ammunition improvements. Representative Caliber . 50 and 20 mm projectiles data appear in the form of computer generated plottings of trajectories for both air to ground and ground to ground roles. Specific information covers time, velocity, and altitude versus range. Projectile characteristics include muzzle velocity, weight and shape with preformance interests centered on time of flight, muzzle velocity and maximum range effectiveness. Air to ground roles include fixed wing and helicopter launchings.

Seven 20 mm and six Caliber . 50 projectiles variations listed in Table I comprised a cross section of nose shapes and weights for the study. Aside from potential application to the air to ground and ground to ground roles these projectiles studies have accumulated quantities of experimental information needed for the study.

Table I Projectile Studies

ITEM	PROJECTILE	WEIGHT GRAINS	NOSE SHAPE
1 2 3 4 5 6 7 8 9 10 11 12 13	20mm M56A3 20mm M56A3 20mm M56A3 20mm PGU-3/B 20mm PGU-3/B 20mm PGU-3/B 20mm M53 Cal50 M8 Cal50 M8 Cal50 M2 Cal50 M2 Cal50 M2	1540 1950 2100 1875 1900 2100 1540 662 850 1130 662 850	Blunt - M505 Fuze Blunt - M505 Fuze Blunt - M505 Fuze Blunt - M505 Fuze Secant Ogive - SAPI Secant Ogive - SAPI Secant Ogive - SAPI Blunt - M505 Fuze Tangent Ogive

METHOD

TRAJE (computer program) is a point mass trajectory program incorporating variation of air density with altitude by means of a subroutine, Atmospheric Computer Program, ATMS1, (1). The basic TRAJE model (2) is

$$m \frac{d\overline{V}}{dt} - \rho(y) A V \overline{V} C_D(V) - \overline{g}$$

m = Projectile weight,

V = Velocity along trajectory, ft/sec

 $\rho(y)$ = Air density as a function of height,

A = Projectile cross section area,

g = Gravitational constant along trajectory

 $C_{D}^{(V)}$ = Drag coefficient as a function of velocity.

Inputs consists of projectile weight and cross sectional area, projectile muzzle velocity and drag curve, vehicle velocity and angle of ascent or descent. Outputs include altitude, range, velocity, time of flight and drag in machine plotted form. Output information is used to compare trajectories, time of flight and velocity decay of various projectiles.

Figure 1 contains curves (3) of drag coefficient versus mach number for projectile items number 1, 4, 7, 8, and 11. Appendix A contains a listing of card types for the program data inputs, and the units for the various parameters. The program is written in Fortran IV for use on the IBM 360 or CDC 6500.

DRAG CURVE VS MACH NUMBER

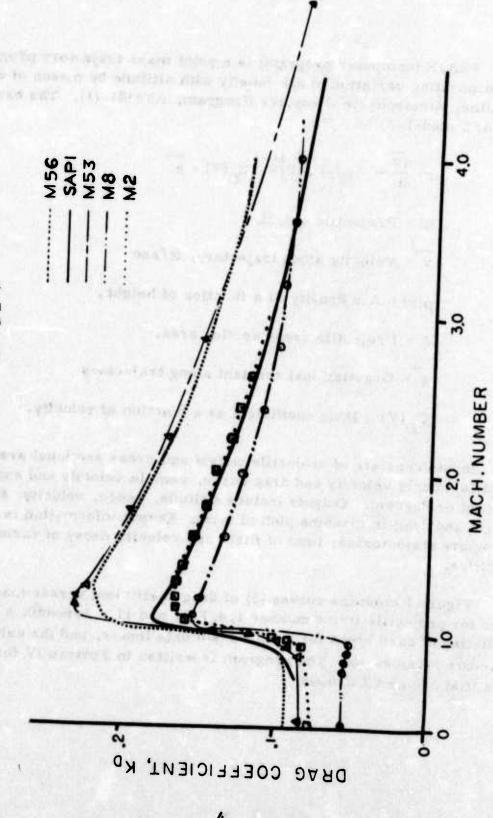


Figure 1. Drag Coefficient Curve

RESULTS

A series of graphs (Appendex C) present the charted data generated during the course of the study for altitude, time, and velocity versus range for each of the projectiles investigated. These graphs present various combinations of the same basic curves to provide comparisons in graphic form. Tables II to V contain listings of these graphs. Table II covers graphs 1 through 27 for 20 mm projectiles launched in the air to ground role at a constant aircraft velocity of 790 knots and a dive angle of 30 from two different altitudes, 182.88 x 10 meters (6000 ft) and 213.36 x 10 meters (7000 ft). The notations in the column headed "drag Curve" refers to the M505A3 fuze or nose shape of the M56A3 projectile as M505 and to the nose shape of the 20 mm PGU-3/B projectile as SAPI. These terms also appear in the legend of the plots and in Table I and are used to identify the drag curve used in the calculations.

Graphs 1 and 2 compare projectiles of two different weights having the SAPI nose launch at two diferent altitudes. Graphs 3 and 4 compare projectiles having the M505 nose shape, same weights, but different muzzle velocities launched at two different altitudes. Graphs 5 and 6 provide the same comparison for projectiles having the SAPI nose shape. Graphs 7 through 12 compare projectiles having M505 and SAPI nose shapes at two weights and three velocity levels launched at two altitudes. Graphs 13 through 16 present a comparison of the M505 and SAPI nose shapes at two launch altitudes by interchanging projectile weights. Graphs 17 and 18 compare SAPI nose shapes at two launch altitudes and projectile weights and three velocities. Graphs 19 and 20 cover the same comparison for the M505 nose shape. Graphs 21 and 22 compare a projectile having the standard M56A3 weight with M505 and SAPI projectiles having the same weights. Graphs 23 and 24 present a comparison of five projectiles, SAPI and M505 projectile nose shapes at two different weights and the standard M56A3. Graph 25 compares the standard M56A3 weight projectile to two heavier M505 and SAPI nose shape projectiles. Graph 26 compares equal weight and velocity M505 and SAPI projectile shapes with standard M56A3. Graph 27 includes the M53 API data for comparison with the M56A, M505 and SAPI nose shaped and weight projectiles.

Table III contains a listing of Graphs 28 through 76 together with identification of the conditions for the graph data. These conditions

differed from those identified in Table II by varying altitude and aircraft speed at lower levels and dive or descent angles. The range selected relates to helicopter launchings. Four projectiles were considered: standard M53, one with M505 nose shape, and two SAPI nose shaped projectiles differing in weight and velocity. Each graph contains four sets of data, one set for each projectile. Table III groups the graphs according to aircraft velocity: Graphs 28 through 37 are for 0 forward velocity while Graphs 68 through 76 are for 200 knots air speed with the other graphs, 38 to 67, grouped for velocities in between.

Table IV lists 24 graphs covering trajectory data for 20 mm projectiles in the ground to ground role at elevations in the 3 to 60 range. Projectiles having M505 and SAPI nose shapes at two velocity levels are compared at one weight level together with the standard M56Al weight projectile. Graphs 77 through 89 cover one velocity level and Graphs 90 through 100 another for the M505 and SAPI nose projectiles.

Table V contains a listing of the graphs presenting Caliber . 50 data. The data involves two Caliber . 50 type nosed projectiles, M2 and M8, launched at three different weights over an elevation angle range of 1 to 60°. Graphs 101 through 120 relate to the M2 data and Graphs 121 through 140 to the M8 data.

out to have a common a second of them will appear the first how

Table II.

20MM Projectiles, Air to Ground Trajectories
Aircraft Velocity 790 Knots, Dive Angle 30°

Graph Humber	Altitude Ft/Motere	Dreg Curve	Weight Grains	Mussle Velocit fpe/mpe
ı	6000/1828.0	SAPI	1950	2950/899.16
	00007 101070	SAPI	1850	3016/919.28
3.00	7000/2133.6	SAPI	1950	2950
2	7000/2133.0		1850	5016
136	7000	N505	1950	3050/929.64
3	7000	M505	1950	2950
4	6000	H505	1950	2950
	6000	H505	1950	5050
5	7000	BAPI	1950	3050
,	70.0	SAPI	1950	2950
	4000	SAPI	1950	2950
6	6000		1950	3050
		SAPI	1950	2990
7	7000	N505		2950
		SAPI	1956	
	6000	SAPI	1950	2950
		H505	1950	2950
•	6000	SAPI	1950	3050
		M505	1950	5050
10	7000	N505	1950	3050
		SAPI	1950	3050
11	7000	M505	2100	2850
		SAPI	2100	2850
12	6000	SAPI	2100	2850
		N505	2100	2850
u	7000	SAPI	2100	2850
		M5 05	1950	2950
		M505	1950	3050
14	6000	SAPI	2100	2850
		H505	1990	3050
		H505	1950	2950
15	7000	N505	2100	2850
		SAPI	1950	3050
		BAPI	1950	2950
16	6000	N505	2100	2850
		SAPI	1950	2950
		SAPI	1950	3050
17	7000	SAPI	2100	2850
		SAPI	1950	5050
		SAPI	1950	2950
18	6000	SAPI	2100	2850
	3000	SAPI	1950	3050
		SAPI	1950	2950
100	Conn		2100	2850
19	6000	N505		2950
		H505	1950	2770

Table II. - continued

Graph Number	Altitude Ft/Meters	Drag Curve	Weight Grains	Mussle Velocity fps/mps
20	7000	M505	2100	2850
		M505	1950	30 5 0
		M505	1950	2950
21	7000	M505(M56)	1540	3350/1021,08
		M505	2100	2850
		SAPI	2100	2850
22	6000	M505(M56)	1540	3350
		M505	5100	2850
		SAPI	2100	2850
23	7000	SAPI	1950	2950
		M5 05	1950	2950
		SAPI	2100	2850
		N5 05	2100	2850
		M505(M56)	1540	3350
24	6000	M505(M56)	1540	3350
		M505	2100	2850
		SAPI	2100	2850
		M505	1950	2950
		SAPI	1950	2950
25	6000	MEVE(MEY)	1540	3350
	6000	M505(M56)		
		N505	2100	2850
	6000	SAPI M505	2100 1950	2850 3050
	0000	SAPI	1950	30 5 0
26	7000	SAPI	1950	3050
	7000	M505	1950	3050
		SAPI	2100	2850
		M505	2100	2850
		M505(M56)		
27	6000		1540	3350
	9000	M505(M56)	1540	3350
		API	2500	2650/807.72
		SAPI	2100	2850
		M505	1875	3016
		SAPI	1875	3016

*NOTE I: The M505 Drag curve was obtained from Ballistic Research Laboratory, Aberdeen, Md and SAPI drag curve was obtained from 20mm API and SAPI Design Review Memorandum, Phase I, October 28, 1969, by AVCO Corporation Ordnance Division.

TABLE III. 2014 PROJECTILES AIR TO GROUND TRAJECTORIES

Weight grains

Muzzle Velocity fps/mps

Drag Curve used

	RIGINO	1 DS7 mps
	1540 2100	3100/944.88 2450/746.36
	2100	2150/ 655.32 2450/74 6.3 6
Altitude feet/meters	Helicopter Velocity knots/fps/mps	Descent Angle
200/60.96	0.0	5°
1000/304.8	0.0	5°
200	0.0	100
1000	0.0	10°
200	0.0	150
1000	0.0	150
200	0.0	30°
1000	0.0	30°
200	0.0	45°
1000	0.0	45°
200	50.0/84.45/57.58	5°
1000	50.0	5°
200	50.0	10°
1000	50.0	10°
200	50.0	15°
1000	50.0	15°
200	50.0	30°
1000	50.0	30°
200	50.0	45°
1000	50.0	45°
200	100.0/168.89/115.16	5°
1000	100.0	5°
200	100.0	10°
1000	100.0	10°
200	100.0	15°
1000	100.0	15°
	200/60.96 1000/304.8 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200 1000 200	Altitude feet/meters

TABLE	III.

continued

Greph Number 54	Altitude feet/meters 200	Helicopter Velocity knots/ips/mps 100.0	Angle 30°
55	1000	100.0	30°
56	200	100.0	45*
57	1000	100.0	45°
58	200	150.0/253.34/172.73	5°
59	1000	150.0	5°
60	200	150.0	10°
61	1000	150.0	10°
62	200	150.0	15°
63	1000	150.0	15°
64	200	150.0	30°
65	1000	150.0	30°
66	200	150.0	45°
67	1000	150.0	45°
68	200	200.0/337.79/230.31	5°
69	1000	200.0	5°
70	200	200.0	10°
71	1000	200.0	10°
72	200	200.0	15°
73	1000	200.0	15°
74	200	200.0	30°
75	1000	200.0	30°
76	1000	200.0	45°

TABLE IV.
20 MM PORJECTILES
GROUND TO GROUND TRAJECTORIES*

Graph	Drag	Weight	Muzzle Velocity fps/mps
Number	Curve	Grains	
77 - 88	M505 (M56)	1540	3350/1021.08
	M505	1950	2950/899.16
	SAPI	1950	2950/899.16
89 - 100	M505 (M56)	1540	3350/1021.08
	M505	1950	3050/929.64
	SAPI	1950	3050/929.64

*ANGLES OF ELEVATION: 3°, 6°, 9°, 12°, 15°, 18°, 21°, 24°, 27°, 30°, 45°, 60°

TABLE V.

CALIBER . 50 PROJECTILES

GROUND TO GROUND TRAJECTORIES*

Graph	Drag	Weight	Muzzle Velocity fps/mps
Number	Curve	Grains	
101 - 120	M2	1033.	2488/758.34
	M2	850.	2910/886.97
	M2	662.	2600/792.48
121 - 140	M8	662.	2910/886.97
	M8	850.	2600/792.48
	M8	1130.	2488/758.34

*ANGLES OF ELEVATION: 1°, 2°, 2.5°, 3° thru 16°, 30°, 45°, 60°

CONCLUSIONS

This report covers a wide range of combinations of drag curve, projectile weight, and muzzle velocities. These parameters in turn effect the time of flight and maximum range of the performance of the various projectiles. It is recommended that similar trajectories be generated for an air to air role as well as other ammunition.

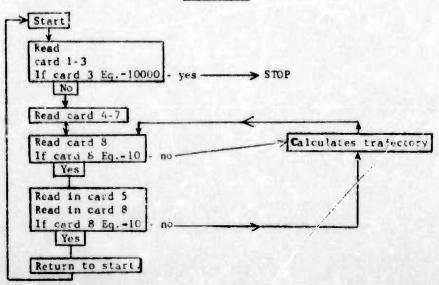
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- 1. U.S. Army Weapons Command, "Some Mathematical Models and Computer Programs for Small Arms Analyses," SY-TN10-80, Ad Hoc Small Arms Systems Analyses Working Group.
- 2. Ballistic Research Laboratories, "Aerodynamic Data for Spinning Projectiles" Report No. 620, H. P. Hitchcock October 1947.
- 3. Engineering Design Handbook, "Design for Control of Projectile Flight Characteristics" AMCP-706-242, Sept 1966.
- 4. BRL Report No. 1628, "Comparative Evaluation of 20 mm Developmental Ammunition (U)", Edited by George Samos, December 1972.

APPENDIX A
TRAJE DATA INPUT AND FLOW CHART

CARD TYPE	COLUMNS	FORMAT	SYMBOL	IDENTIFICATION	UNITS
1	1 - 7	F7.4	P	pressure	cm hg
	8 - 14	F7.4	TEMP	temperature	of
2	1 - 24	6.4	SHAPE	projectile shape	
3*	1 - 6	F6.3	V (1)	velocity	
	7 - 14	F8.5	CD(1)	drag coefficient	
4	1 - 7	F7.2	DVV	velocity	interval
5	1 - 7	F7.2	Y(1)	altitude	meters
6	1 - 10	F10.5	G	gravity	m/sec
	11 - 20	F10.5	A	cross sectional area	in ²
	21 - 30	F10.5	XM	mass	grains
	31 - 40	F10.5	ANGO	angel of descent or ascent	radians
	41 - 50	F10.5	VI	muzzle velocity	fps
7	1 - 7	F7.4	W	wind velocity	mps
8	1 - 6	F6.2	VPLANE	aircraft velocity	fps

FLOW CHART



* Note: card type 3 is a set of cards containing the points of the drag curve with the last card being -10.

APPENDIX B

COMPUTER PROGRAM LISTING

```
PROGRAM TRAJE(INPUT.OUTPUT.TAPE1=INPUT.TAPE3=OUTPUT.TAPE4)
      REAL LOT
      DIMENSION SHAPE (6)
      (005) ACLIENT (005) CO. (005) ADMANOISMAN (005)
      COMMON Y(200) . T(200) . V(200) . CD(200) . K . I . X(200)
      COMMON VV(2001.CC(200).VPLANE
      COMMON 27 (200)
    5 FORMAT (6A4)
    6 FORMAT (20x - 19H MUZZLE VELOCITY # + F5.0 - 7H FT/SEC )
    7 FORMAT ( 14 . 247)
    P FOR 4AT (2F5.2)
    G FORMAT (2AS)
   25 FORMAT (1H1. 10X. 70H ANGO (MILS). D(LBS/FT3). PRES (IN). TEMP (F)
     A XM (GRAINS) VI(FT/SEC)
   27 FORMATI 25H WIND VELOCITY (M/SEC) = + F7.4. 12H PRESSURE = +F7.4.
     218H TEMPERATURE (F) = . F7.4)
   44 FORMAT(10X. 10H Y(METERS). 9X.11H X(METERS). 13X. 7H T(SEC). 6X. 1
     24H V(METERS/SEC) . 16X . 4H CD . 9X . 11H Z(METERS) )
   45 FORMAT(1X.3F20.8)
   46 FOHMAT(1X-10H ALTITUDE +10X+ 9H DENSITY + 11X+ 13H TEMPERATURE +7
     2×1
   55 FOMMATI 5F20.81
   56 FORMAT (5F16.8)
   57 FOWMAT(100X.3F10.4)
   SE FORMAT(1x.6F20.8)
   60 FORMAT (11H DENSITY = +F7.6. BH TEMP = +F10.4.10H HEIGHT = +F10.4)
   61 FORMAT (1H1)
6P FORMAT(SF10.5)
   69 FORMAT ( 15x + 4E15.8)
   75 FORMAT ( 14H FORCE (NTS) =+E16.6. 15H YDOT (M/SEC) =+E16.6. 16H VEL
        (M/SEC) = .E16.6)
   HO FOHMAT (14H VEL (M/SEC) = + 14X + 7H CD = + 20X)
   81 FOW AAT (17.4F15.8)
  102 FORMAT (15F5.0)
103 FORMAT (1H1. 61A1)
  106 FOW MAT (F7.2)
  202 FON MAT (2F20 . H)
  203 FORMAT (F6.2)
  204 FORMAT (F6.3.F8.5)
  205 FORMAT (3F7.4)
  428 FORMAT (18H PLANE VELOCITY =+ F6.0+34H FT/ SEC AT AN ANGLE OF DESC
    TENT OF . F6.4. 9H HADIANS.)
  528 FORMAT (46H INPUT IS REL PROJ VEL IN FT/SEC. DRAG COEF KD.)
 1000 FOR 1AT (3A1)
 1010 FORMAT( 11H WT OF PROJ.F14.8. 11H NOSE SHAPE.A5)
 1011 FORMAT(13H MUZZLE VEL= . E14.7. 8H FT/SEC )
 1012 FORMAT (1X+6A4)
 1013 FOWMAT(IX-E14-8-19H WT. OF PROJECTILE )
  1 PRESSURE TEMPERATURE (2F7.4)
    2 SHAPE (644)
Cassasse
             3
                  VV(J) (FT/SEC) +CC(J) (KD)
                                                     F6.3.F8.51
            DVV(INCREMENTS/VELOCITY)
                                                  (F7.2)
            Y(1) (ALTITUDE)
                                        (F7.2)
           GIGRAVITY-METERS PER SECONDS SQUARED .AICROSSSECTIONAL AREA)
     6
      .XM(MASS-GHAINS) . ANGO (ANGLE OF DESCENT OR ASCENT. VI (MUZZLE
    7 WIND VELOCITY (F7.4)
    A AIRCRAFT VELOCITY (F6.2)
     9 ALTIUDE ** FOR SAME AIRCRAFT VELOCITIES CAN RUN AT VARIOUS ALTI-
                   TUDES. TO CHANGE AIRCRAFT VELOCITY PUT -10. FOLLOW
                    WITH ALTITUDE AND THEN AIRCRAFT VELOCITY WILL RETURN
                    ASKING FOR ALTITUDE AGAIN **
   10 -10. PLACED FOR LAST AIRCRAFT VELOCITY. -10. PLACED FOR LAST G
C N=NUMBER OF TIME INTERVALS
```

C

C

```
C DT=TIME INCHEMENTS (SEC)
C DT=TIME INCHEMENTS (SEC)
C VELDY=DECREASE IN VELOCITY DUE TO DRAG/DRAG VEL IN Y DIRECTION (M/SEC)
C AV=AVERAGE DECELEMENTION (VEL) DUE TO DRAG (M/SEC)
C AV=AVERAGE DECELEMENTION (VEL) DUE TO DRAG (M/SEC)
C AV=AVERAGE DECELEMENTION (VEL) DUE TO DRAG (M/SEC)
         ATMS1 (YHEALTITUDE (FEET) . TEMP (RANKINE) .PRES (SLUG/FT*+2.
C DENSITY= SLUG/FT++3)
     A= CROSS-SECTIONAL AREA FOR 20MM (EITHER .515 OR
C C=CONSTANT
C ANGE ANGLE OF TRAJECTORY . YDOT = Y VELOCITY .DX=CHANGE IN X DISTANCE
C X(1)=X DISTANCE . AV = AVERAGE VELOCITY . Y(1)= Y DISTANCE
C VEL= FT/SEC . *O DRAG CURVE
C VEL= FT/SEC
C 7 IS WIND VELOCITY EFFECT ON PROJECTILE
C** TEMPERATURE IN F
C** PRESSURE CM OF MERCURY
C**** WE WIND VELOCITY IN METERS PER SECOND
C ** IF VELOCITY (FPS) AND KD CURVE
C** VV(J) = VV(J) /3.2809
Coo
       201 CC(J) *CC(J) *8./3.14159
C. IF INPUT VELOCITY (MACH) AND CD CURVE
       SPS0=SQ4T((959.67 + TEMP)/518.67)*340.294
C.
        VV (J) = VV (J) + SPSO
C++
C++ 201 CONTINUE
        INEI
        10=3
     ? CONTINUE
        REAU (IN. 206) P. TEMP
        READ (14.5) SHAPE
        SPS0=SQRT ((459.67 . TEMP)/518.67) #340.294
       00 201 J=1.200
HEAD(IN.204)VV(J).CC(J)
        IF (VV (J) . LE . - 9.) GOTO228
        1F (VV(J) .GE . 10000 . ) GOTU40
        VV(J) = VV(J) +SPS()
   201 CONTINUE
   I-L=M ASS
       DV=VV(1)
        N=VV(1)/19.
        N.2=L0200
        OV=DV-IO.
        CALL INTERRICC . CD (J) . DV . VV . K)
        V(J)=DV
    20 CONTINUE
        V(1) = VV(I).
        CD(1) =CC(1)
        WRITE (10.25)
        KKK=0
        DO 1001 J=I+4
        (L) V= (L) VV
        CC(7) =CD(1)
 1001 CONTINUE
        READ (IN. 106) DVV
    21 CONTINUE
        READ (1N. 105) Y(1)
        IF (Y(1) .LE.-10.) GOTO17
        GOTO15
    I7 CONTINUE
        READ(IN-106) Y(1)
        READ (IN. 203) VPLANE
        IF (VPLANE.LE.-10.) GUTO19
    IA CONTINUE
        IF (KKK.GE.1) GOTO24
    19 READ (IN-68) G.A.XM.ANGO.VI
        IF (G.LE.-IN.) GOTO2
READ (IN. 206) W
        WRITE (10+27) W.P. TEMP
```

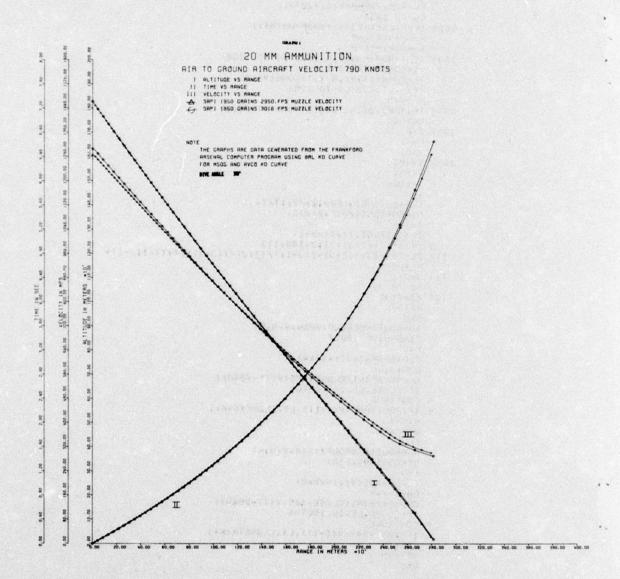
```
WRITE(10+1012)5HAPE
   WRITE(10+1013)XM
   VMUZ = V1
   XM = XM/7000.
   ANGO = ANGO - .001
   WRITE(10.1011)V1
24 READ (IN. 203) VPLANE
24 CONTINUE
    WRITE (10.428) VPLANE . ANGO
    VI=VMIJZ
    V1 = (VI + VPLANE)/3.2808
    CALLGROUP (VI.VV.N.1)
    K=N-1+1
    DO 324 J = I+K
    L=1.J-I
    CD(J)=CC(L)
324 V(J)=VV(L)
S8 VELUY = 0.
    V(1) = VI
    T(1) = 0.
    x(1)=0.
    ANG = ANGO
    K1=V(I)/I0.
    DVI=DVV/10.
    IDV=DV1
    K=1
    C2=1.6494/144./XM
    vi)1=0.
    DV=DVV
    201=0.
    /7(1)=0.
    7=11.
    D0131=2.41
    21=1-1
    K=K+IDV
    KK=K-IIIV
 30 YH=3.281#Y(1-1)
    1F(YH.LE.O.) GUTO31
    CALLFOOID (YH . TEMP . PHES . D . VIS . VELA . 0)
    001035
 31 0=.00237
 32 0=32.1739+0
     TEMP=TEMP - 459.69
     C=C>+D
     VBAH=(V(1) + V(I-1))*.5
     ANG I = ANG
     ANG=ANG-.0005
     1F (ANG.LT.-1.5) GDTD40
221 CONTINUE
     D1=2.*(I./(v(1)-x1*DV)-1./(v(1)-(x1-1.1*DV))/C/(CD(1)+CD(I-1))
     DT= DT + 2./C/(CD(1) + CD(1-111*ALOG(COS(ANG1)/COS(ANG))/VBAR
AV=.5*(CD(1)*(V(1) - XI*DV1**2*SIN(ANG) + CD(1-1)*(V(1) - (X
    21-1.01*DV) **2*SIN( ANGI)1
T(1)=T(1-1) • DT
VELOY= VDI + C*AV*DT/2.
     ANG2=ANG
     YDOT= -VELDY -G+T(1) + V(1)+S1N(ANGO) - C+AV+DT/2.
     ANG=ATAN (YDOT/(V(1)-X1+DV)/CDS(ANG))
     1F(AHS(ANG2 - ANG) .LE. .001*ABS(ANG))GOT0224
     GD1022I
 224 VDI= VELDY + C*AV*DT/2.
 222 CONTINUE
    X(1)=DX + X(1-1)

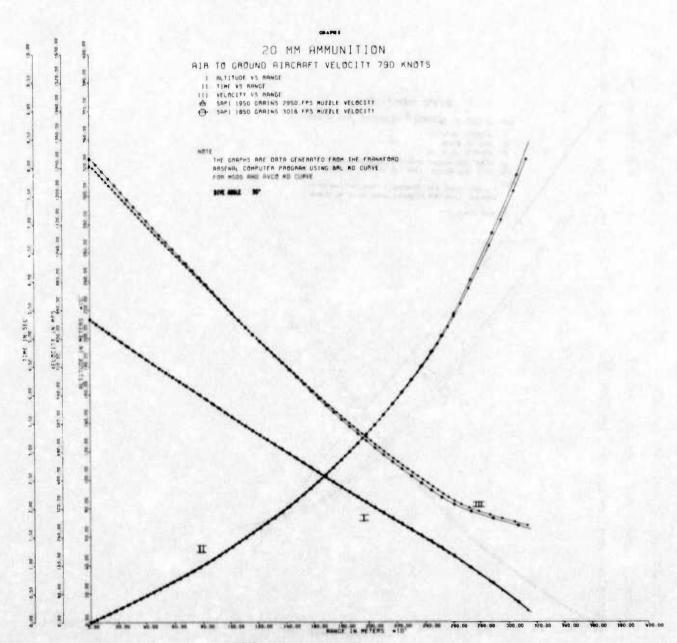
Y(1)=Y(1-1) - .5*(G*(T(1) + T(1-1)1)*DT - VELDY*DT +DT*V(11*SIN(A))
```

```
+ CD(1-1)*(V(1) - (X1-1.)*DV))*2.25
      CHAHS C+ (CD(1)+(V(1)-X1+DV)
      ZD= w+ (ZD1 - W)*EXP(-CHAR*DT)
Z= Z + W*DT + (ZD1 - W)/CHAR*(1.-EXP(-CHAR*DT))
      201=20
      ZZ(1)=Z
      ANGA(1) = ANG
      CO(1)=C
      VELUA(1) = VELUY
      1F(Y(1))11.12.12
  12 1F(V(1).LE.0.)G01011
      1F(1.GE.200)G01011
  13 CONTINUE
   11 WRITE (10.44)
      1=1-1
      00103=1-1
      WRITE(10.58) Y(J).X(J).T(J).V(J).CD(J).ZZ(J)
   IN CONTINUE
      KKK=KKK.)
      120109
   40 STOP
      END
      SUHROUTINE FOOID (H.T.P.R.VK.VS.IDPT)
     FOOLD WAS PREVIOUSLY ATMST
C
      DIMENSION HH (12) +W1(11) +W2(11) +W3(11) +TB(11) +PB(11) +RB(11)
      DIMENSION A(3) .B(3) .C(3) .D(3)
  350 FORMAT (51H0112547537990105160170200700-225569-525612000157689./
     162H13846611388300U120869-159202-759218000206234241458854120886289+
     260H170H24075434134164803507156832960222129976137005186882116217./
      3574237692389988472730706238998805197977655087880002515528804.
      426H50878800012181139468298188. /
      561H2108411892981882180942614061881556222322386188757818452566188.
      6604589541338283618829759611330486356766490205762269881987291000./
      73447595111741642200259357872739661814)
  351 FORMAT (F1.0.-3P6F2.0.5F3.0. 10PF7.0. 5PF7.0.0P3F1.0. 9PF6.0./
      1 10PF6.0. 4PF6.0.0P3F1.0. 9PF6.0. 10PF7.0. 5PF7.0.0P3F1.0. 9PF6.0
      2 . 10PF6.0. 4PF5.0.0PF1.0. 10PF6.0. 5PF6.0.0PF1.0. 11PF6.0. 5PF6.0
      3 .0PF1.0. 11PF6.0. 5PF6.0.0PF1.0. 11PF6.0. 5PF6.0.0PF1.0.3P2F7.0./
4 RPF6.0.3P2F6.0.7PF4.0.3P2F6.0.8PF4.0.4P2F7.0.10PF5.0.
      5 4P2F7.0.11PF6.0.3PF6.0./5PF4.0.12PF5.0.
      6 3PF6.0.7PF5.0.12PF4.0.3PF6.0.8PF5.0.13PF4.0.3PF7.0.9PF4.0.15PF4.0
      7 .3PF7.0.10PF5.0.15PF4.0.3PF7.0.10PF5.0.16PF4.0.4PF4.0.0PF7.0.
      8 6PF8.0.13PF6.0.2PF5.0.-4PF1.0.0P4F1.0./6P2F6.0.-3P2F3.0.6P2F6.0.
      9 -4P2F2.01
   352 FORMAT (1x.F3.2.11F10.0./22(1x.3E20.10/).F8.4.F10.0.F10.6.E20.8.
      1 FH.2.F10.0./1x.4(F5.2)/1x.2F10.6.2F10.0./1x.2F10.6.5X.2F10.0)
  2001 FORMAT (1X+5HALT= +E9+4+12H BELOW L1M1T)
       1F (1TAPE.EQ.4) 60 TO 5
       ITAPE=4
       REWIND ITAPE
       WRITE (ITAPE . 350)
       REWIND TTAPE
       READ (1TAPE+351) (HB(1)+1=1+12)+(W1(1)+W2(1)+W3(1)+1=1+11)+(TB(1)+
      1 PH(1) +RB(1) +1=1+11) +CUN1+CON2+CDN3+CON4+CON5+CON6+(A(1)+B(1)+C(1)
      2 .0(1) . 1=1.3)
     5 CONTINUE
       HGP=CON1 @H/(1.+(CON1 @H/CUN2))
       IF (HGP.LT.O.) HGP=0.
       00 1002 M=1.11
       1F (HGP-HH (M))1003.1004.1002
  1002 CONTINUE
       IF ((HGP-HH(12)).GT.O.) GO TO 1052
       M=12
  1003 M=M-1
  1004 TM=T8(M) # (1.+W1(M) # (HGP-H8(M)))
       1F ((HGP-90000.).GT.O.) GO TO 1006
```

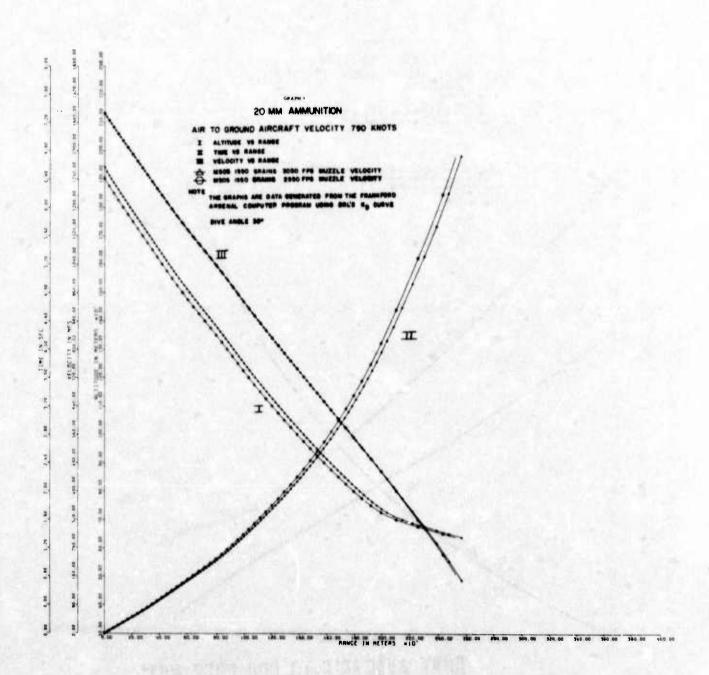
```
THIM
     GO TO 1070
1006 IF ((HGP-180000.).GT.O.) GO TO 1009
     1=2
     GO TO 1007
1009 1=3
1007 T=TM#(A(1)-B(1) #ATAN((HGP-C(I))/D(I)))
1070 1F (W2(M))1011.1020.1011
1011 TEMP=1 . + W1 (M) . (HGP-H8 (M))
     P=PH (M) / TEHP ** #2 (M)
     R=HB(M)/TEMP**(1.+W2(M),
     GO TO 1030
1020 TEMP=EXP(-w3(M) + (HGP-IIB(M)))
     PEPH (M) #TEMP
     R=HA (M) #TEMP
1030 IF ((HGP-CON6) .GT.0.) GO TO 1032
     VS=CON3*SQRT (TM)
     VK=CON4*(T**1.5/((T+CON5)*R))
     1F(H.LT.0.) GO TO 1050
     RETURN
1050 IF (10PT.GT.0) WRITE (JOUTPT.2001) H
     RETURN
1052 T=0.
     P=0.
     H=0.
1032 VS=0.
     VK=0.
     RETURN
     END
     SUBROUT INEINTERR (Z.ZZ.TT.T.J)
     01MENS10NT (200) +2(200)
     A=1.
     1F(T(1) .GT.T(2)) A==1.
   3 1F(A+(TT-T(J)))112+100+113
 112 ZZ=Z(J-1)+((Z(J)-Z(J-1))/(T(J)-T(J-1)))+(TT-T(J-1))
     RETURN
 113 J=J+1
     60 TO 3
 100 ZZ=Z(J)
     RETURN
     END
     SUBROUT INEGROUP (VBAR+V+N+K)
     DIMENSIONV(200)
     K=0
     CLOSE=ABS(V(1)-VBAR)
     D051=1 . N
     CLUSE=AMINI(CLOSE+ABS(V(1)-VBAR))
     IF (CLOSE.LE.10.) GOTO6
   5 CONTINUE
   6 IF (ABS (VBAR-V(I+1)) .LT.CLOSE) K=K+1
     K=K+1
     RETURN
     END
     SUBROUT INEGROUP (VBAR+V+N+K)
     DIMENSIONV (200)
     K=0
     CLOSE=ABS(V(1)-VBAR)
     0051=1.N
     CLOSE = AMINI (CLOSE + ABS (V(I) - VBAR))
     IF (CLOSE .LE. 10.) GOTU6
   5 CONTINUE
   6 IF (ABS (VBAR-V(I+1)) .LT.CLOSE)K=K+1
     K=K+1
     RETURN
     END
```

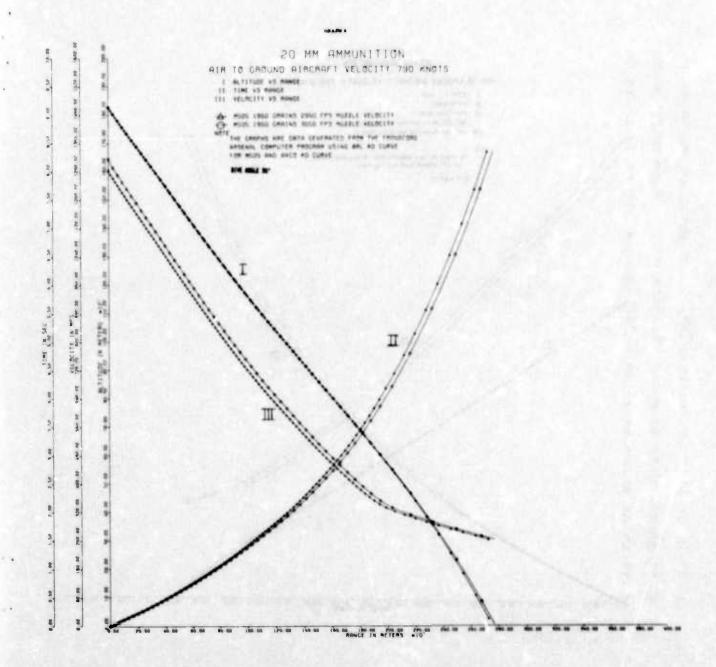
APPENDIX C Graphs 1 to 140: 20MM and Caliber 50 Trajectories

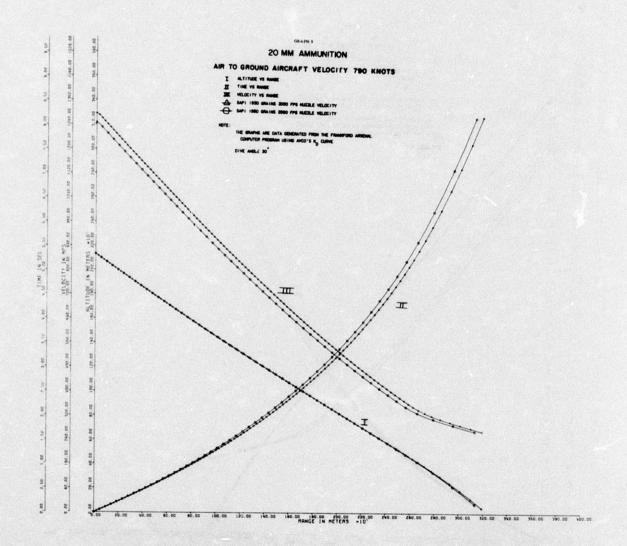


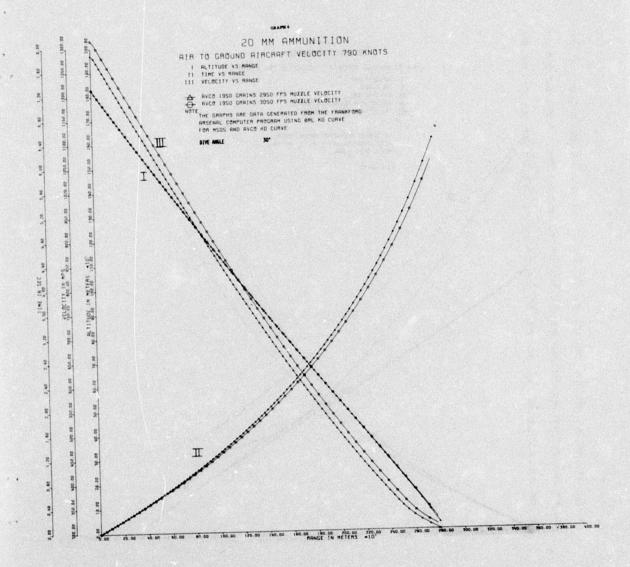


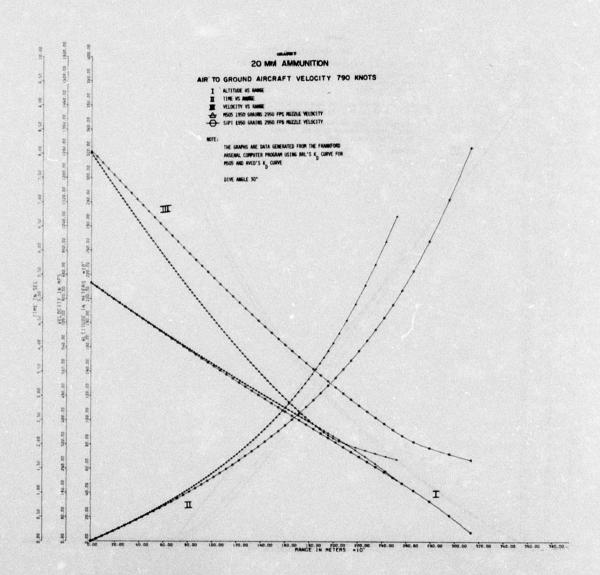
COPY AVAILABLE TO DDC DCES NOT PERMIT FULLY LEGIBLE PRODUCTION

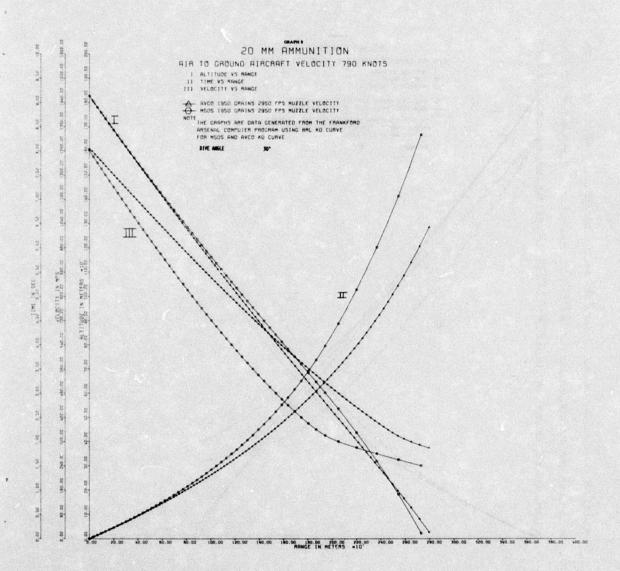


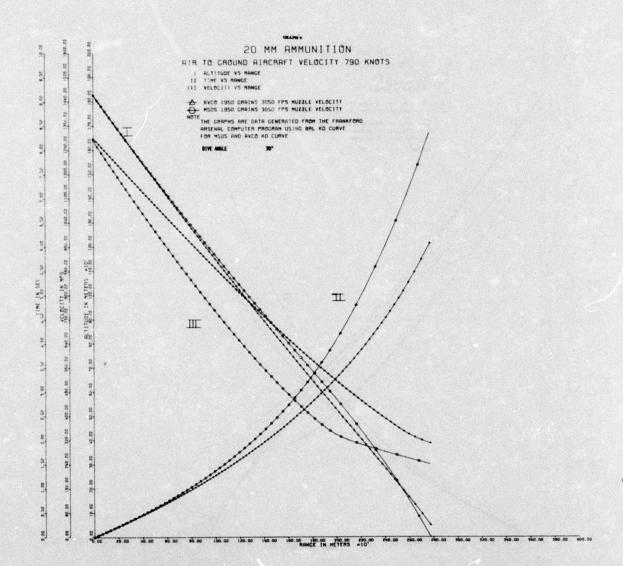


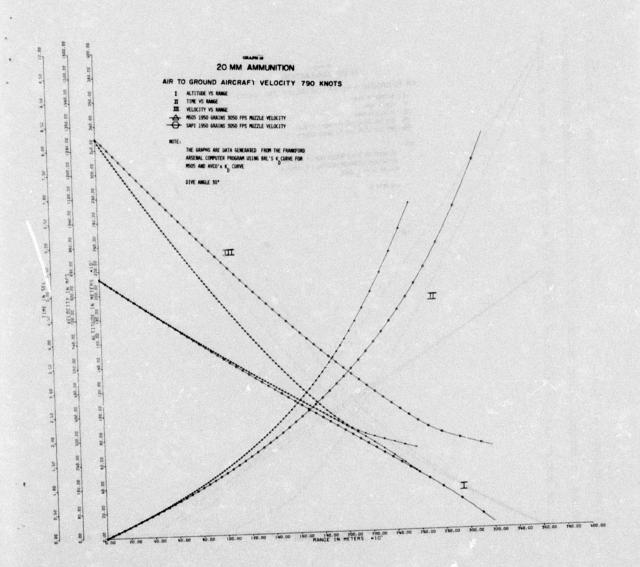


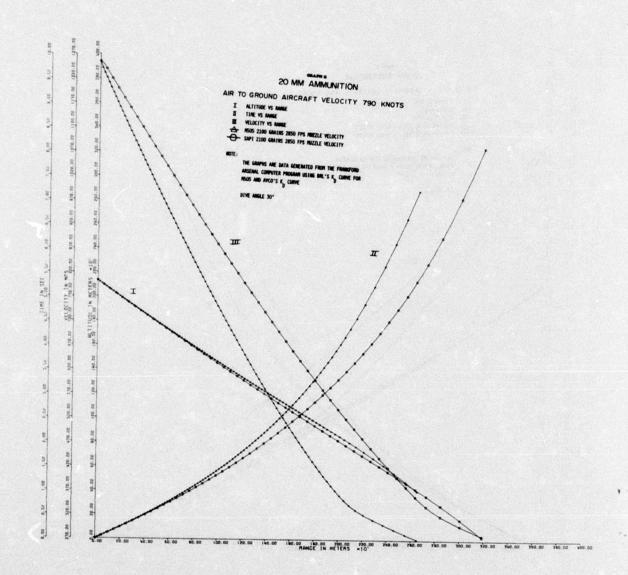


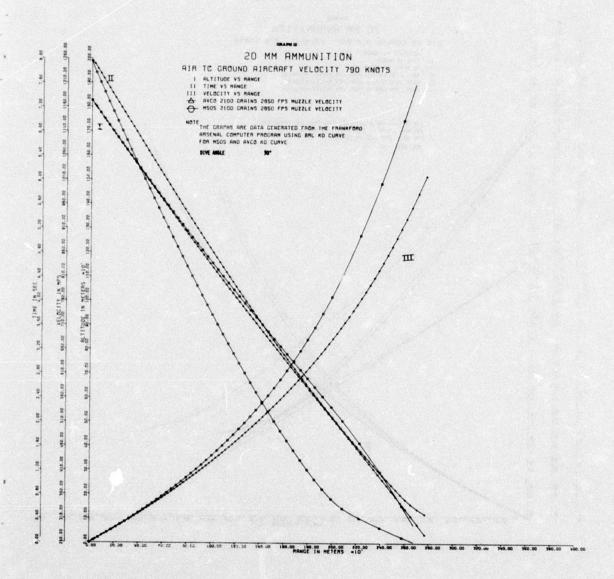


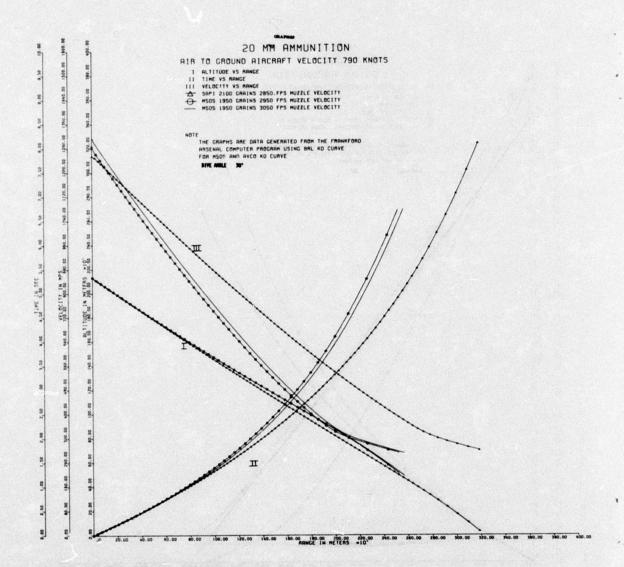


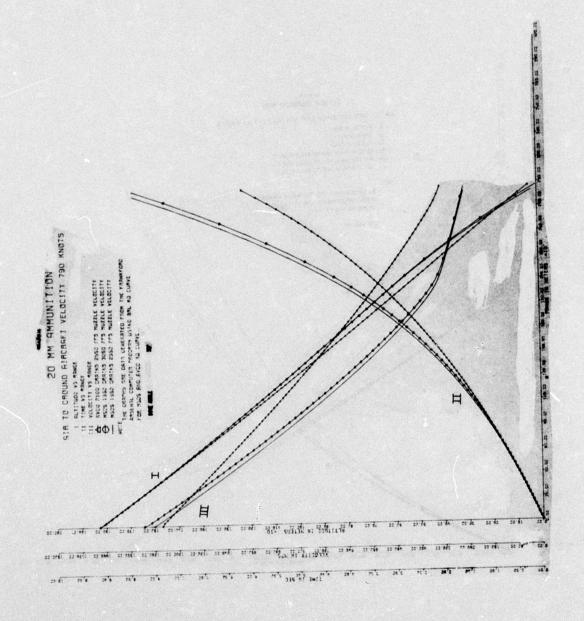


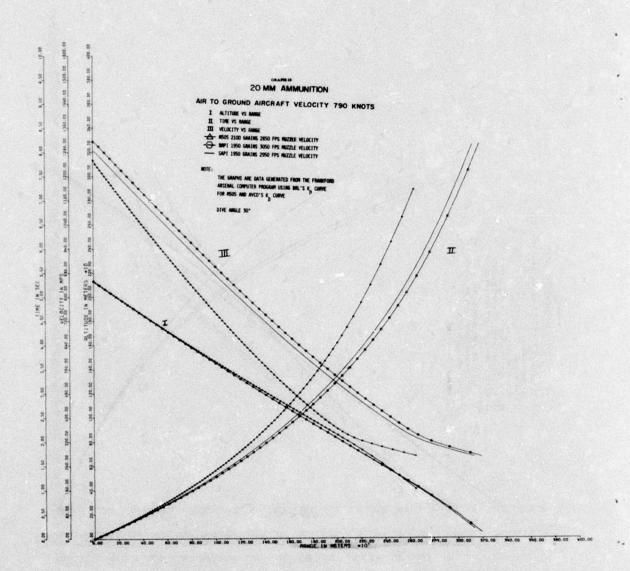


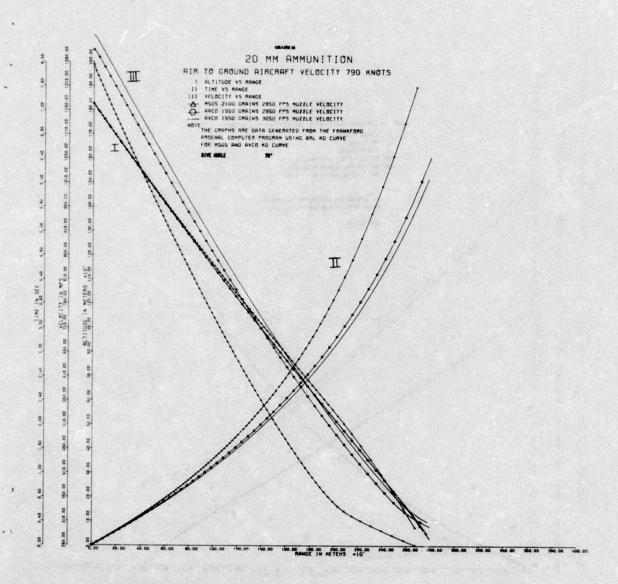


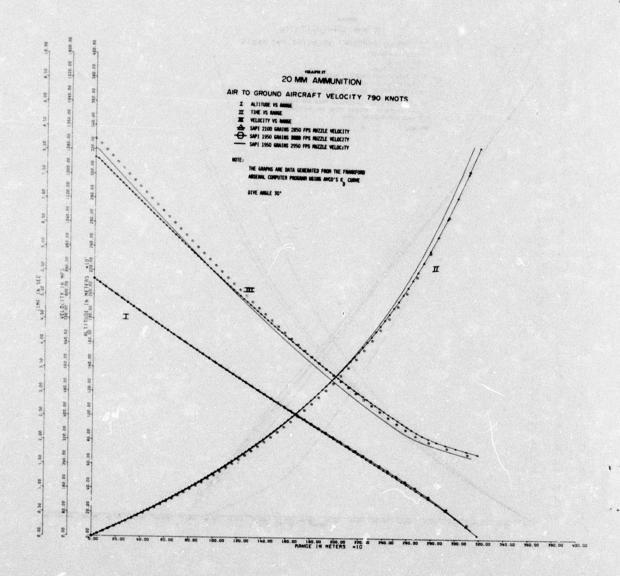


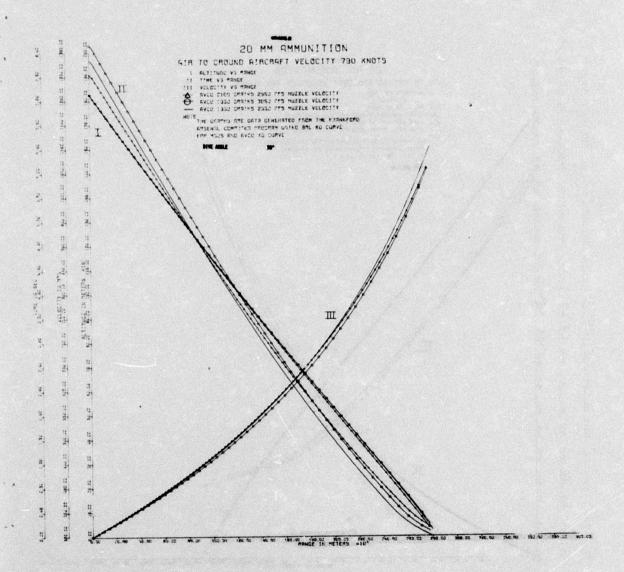


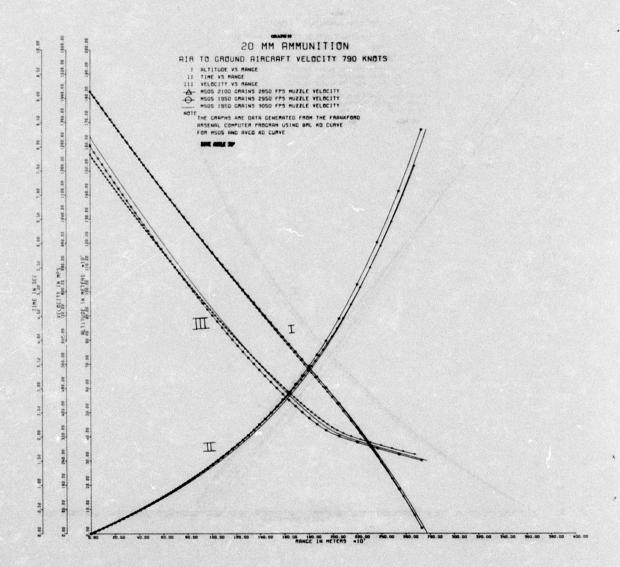


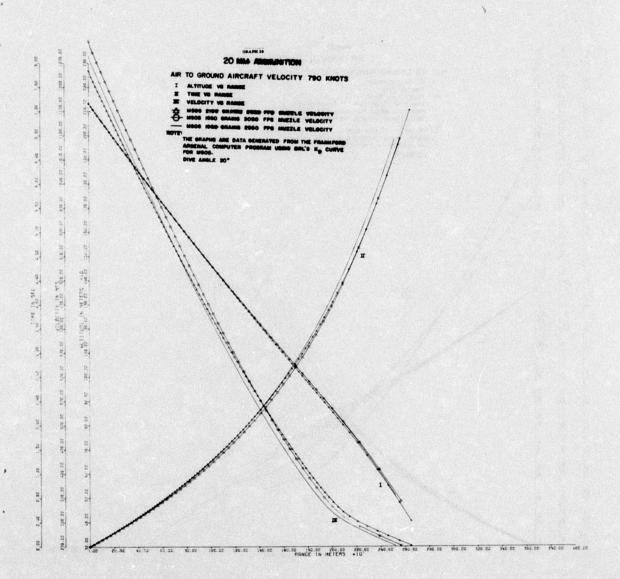


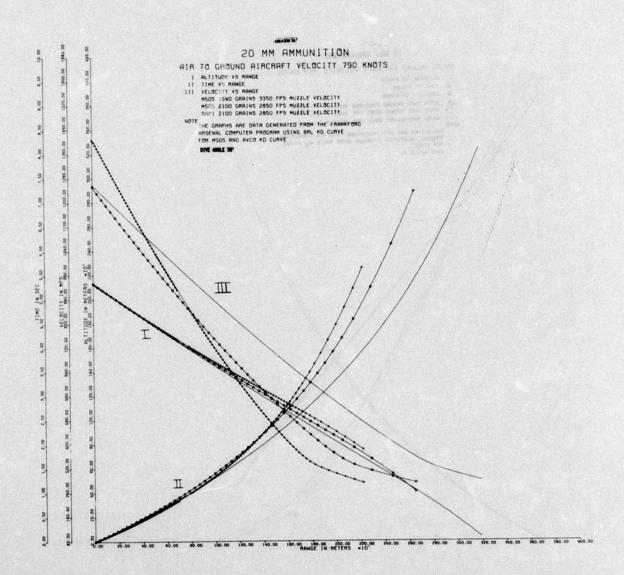


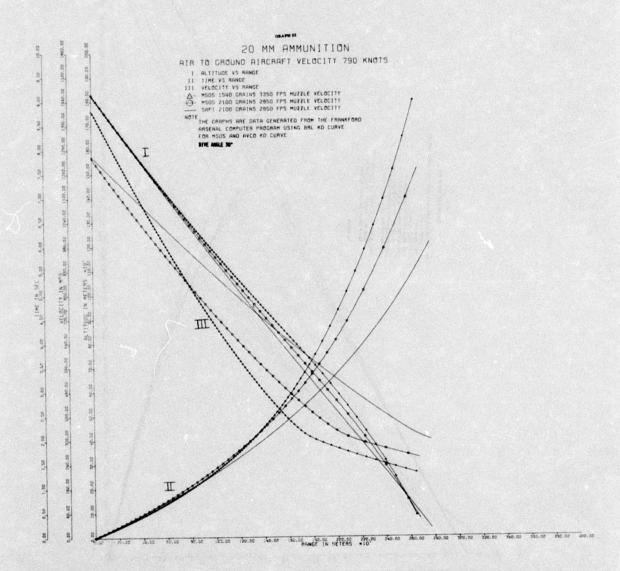


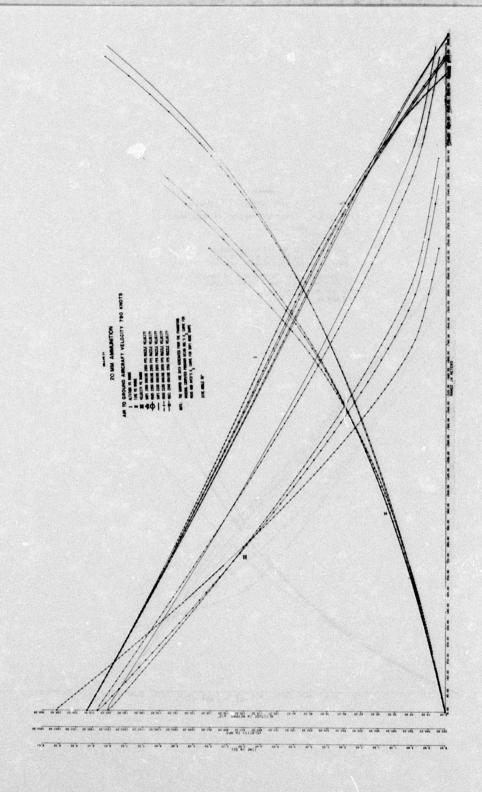


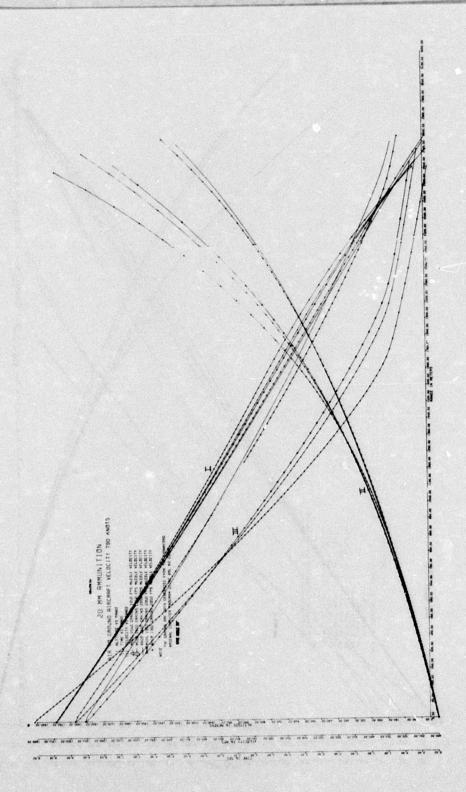


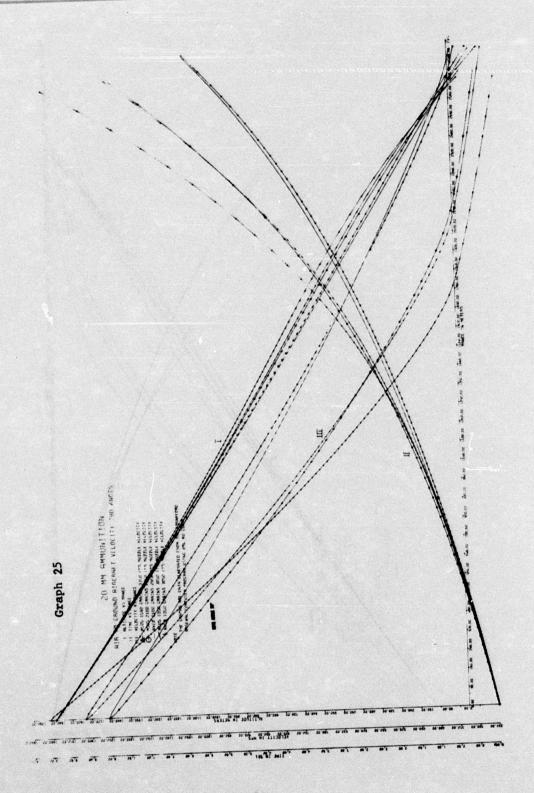


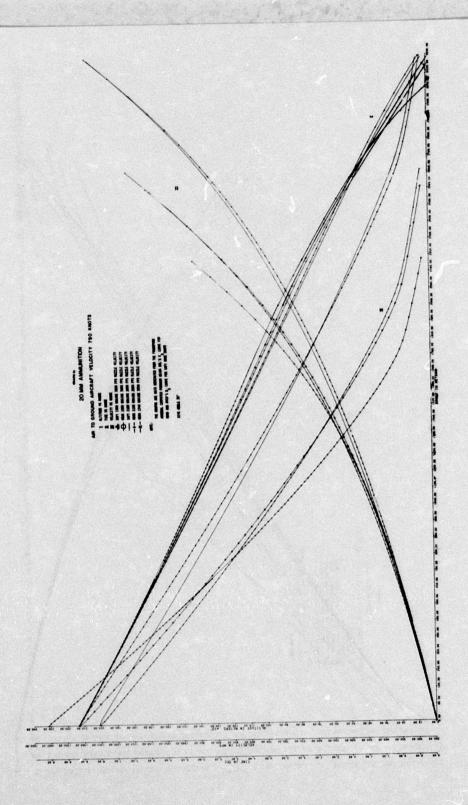


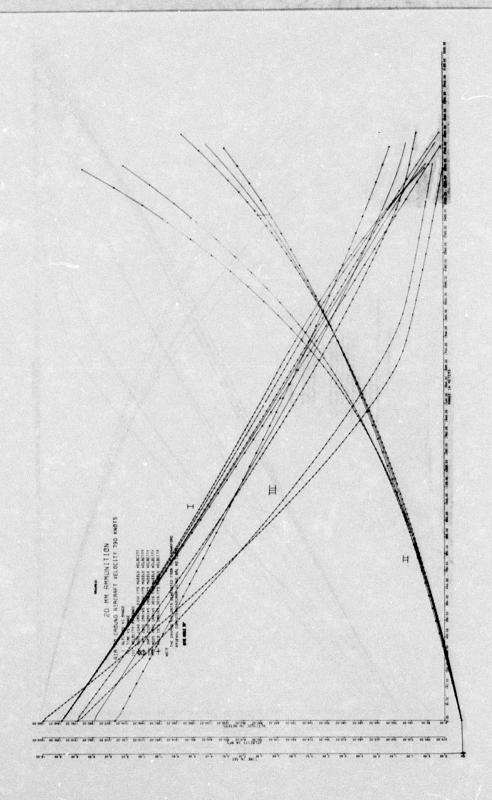


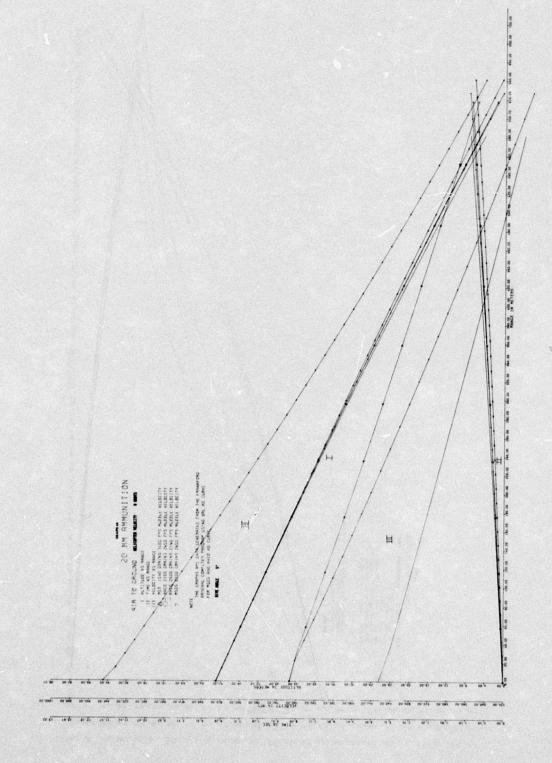


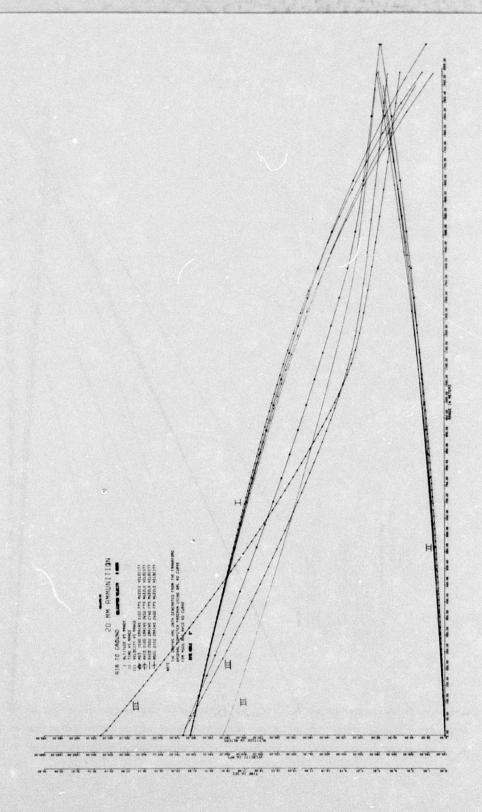


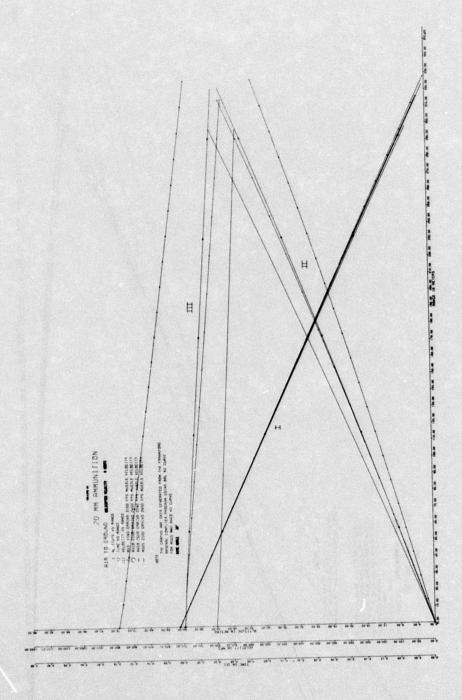


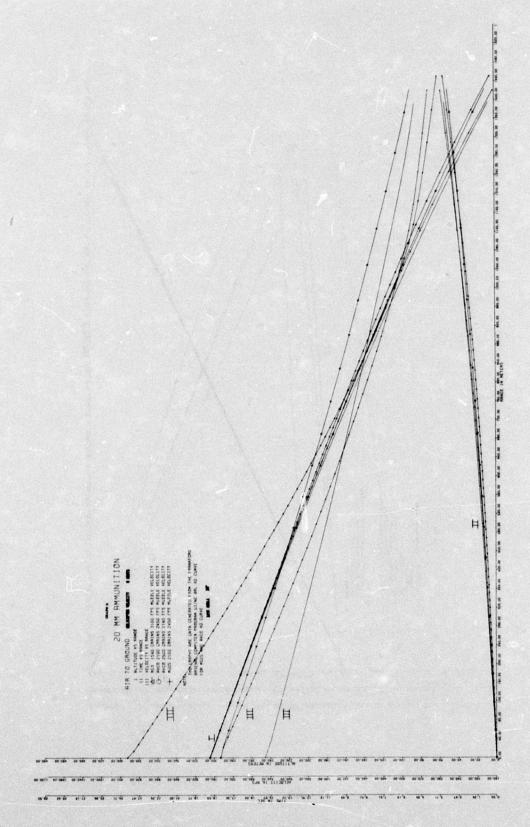


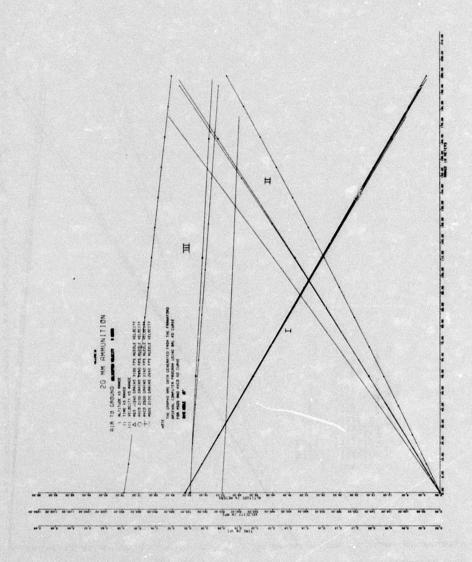


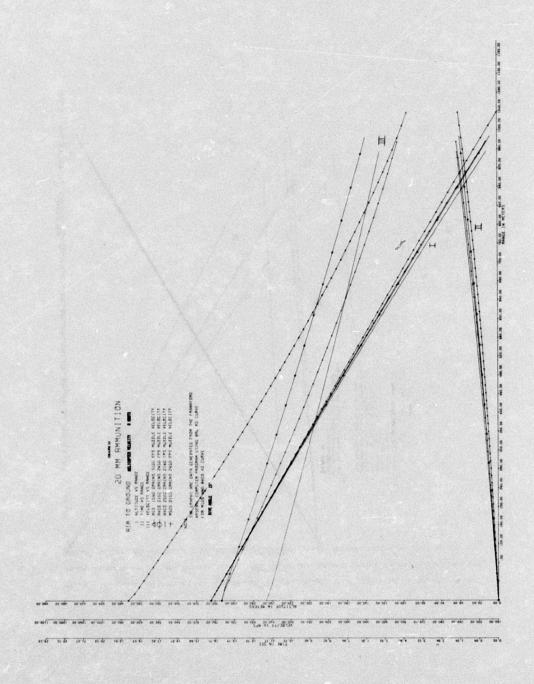


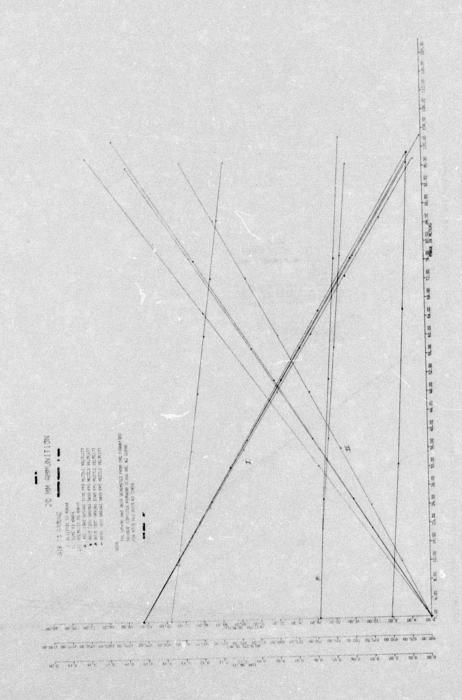


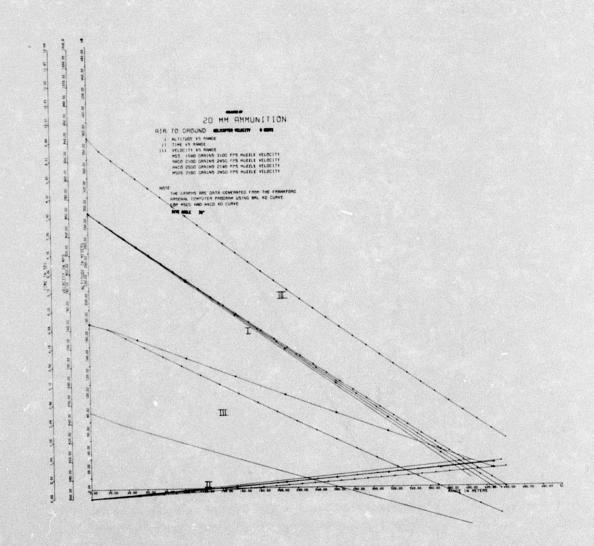


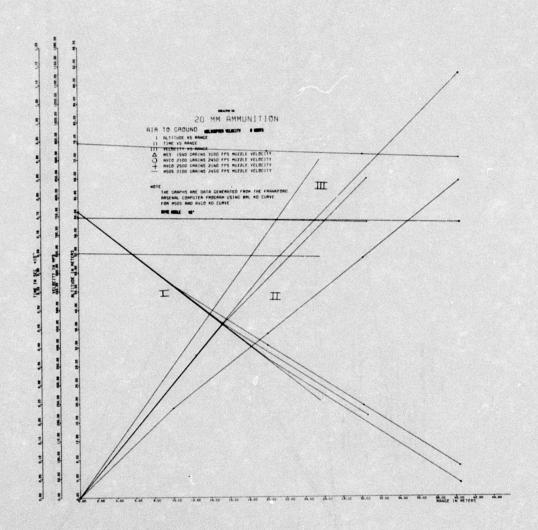




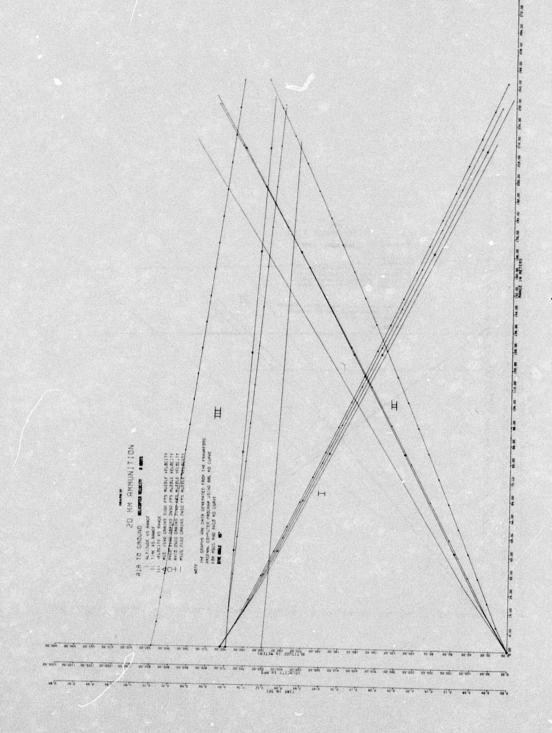


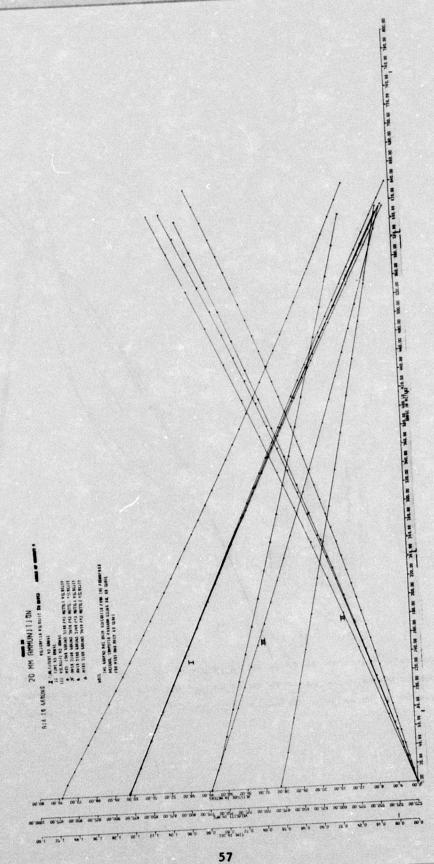


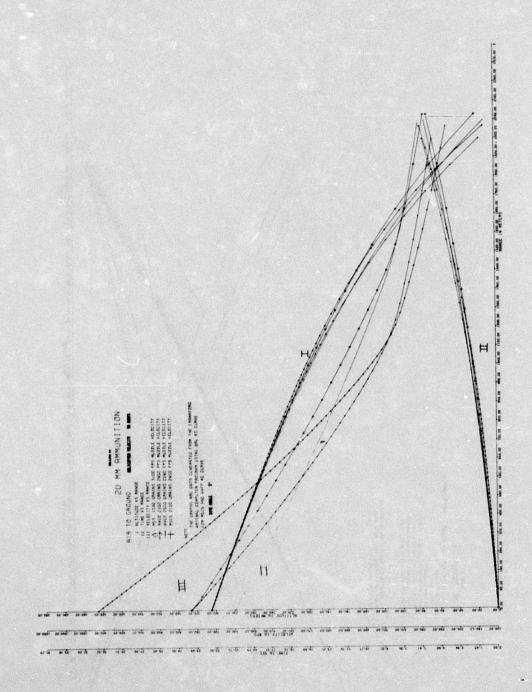


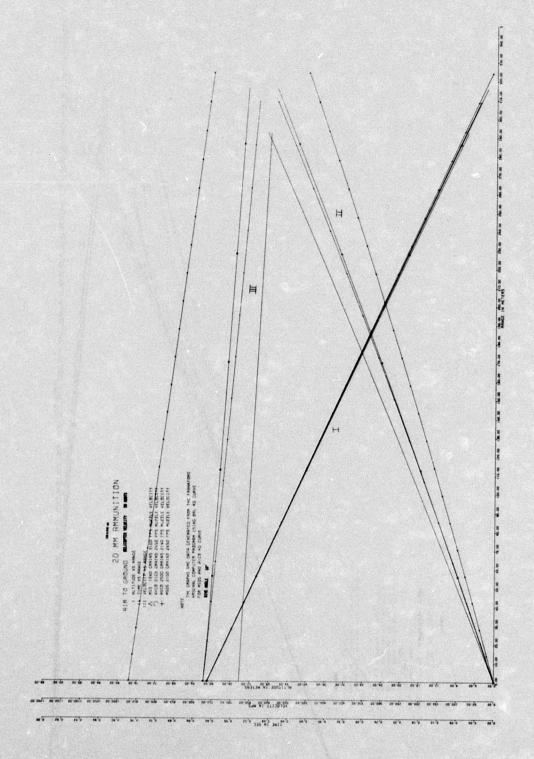


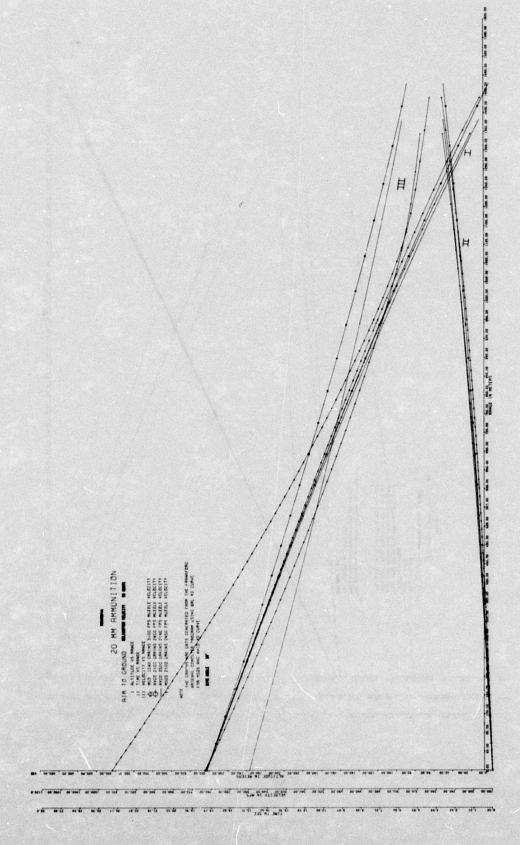
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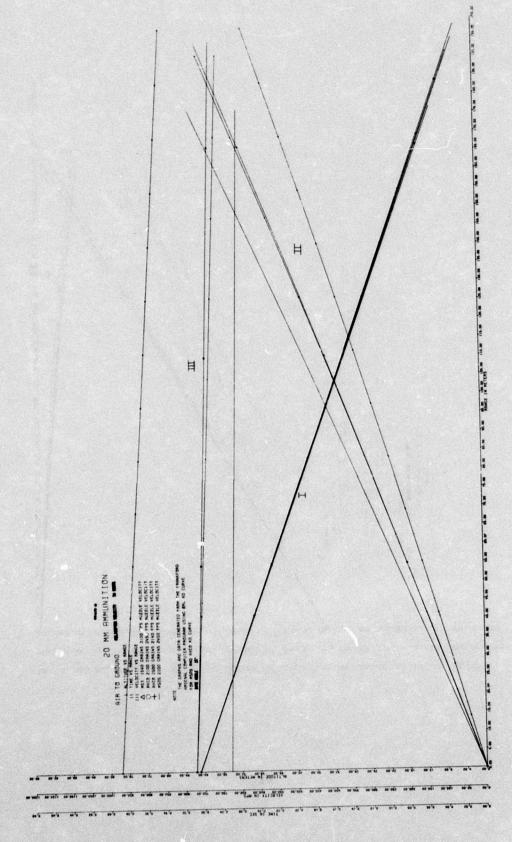


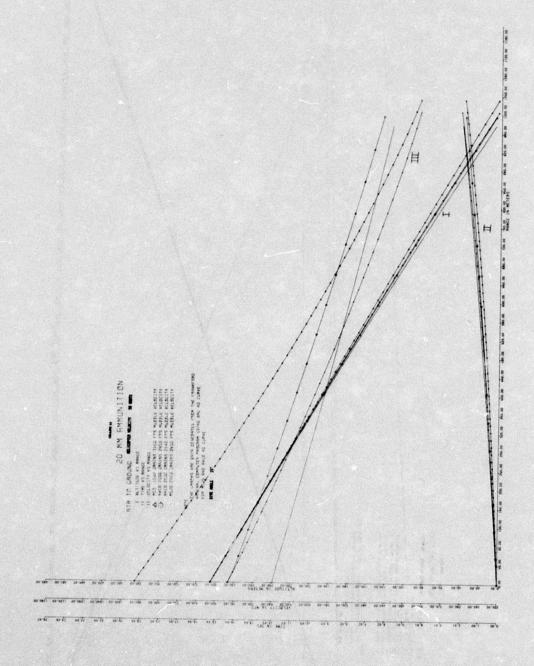


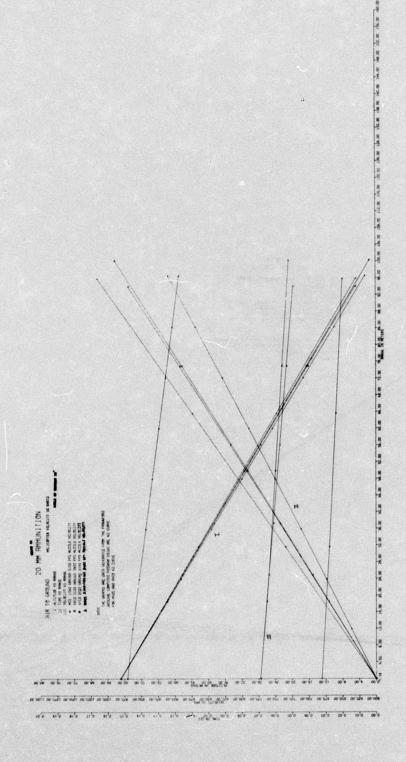


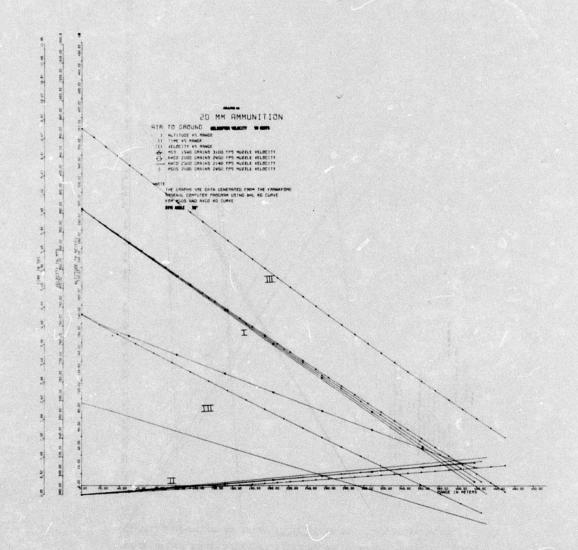


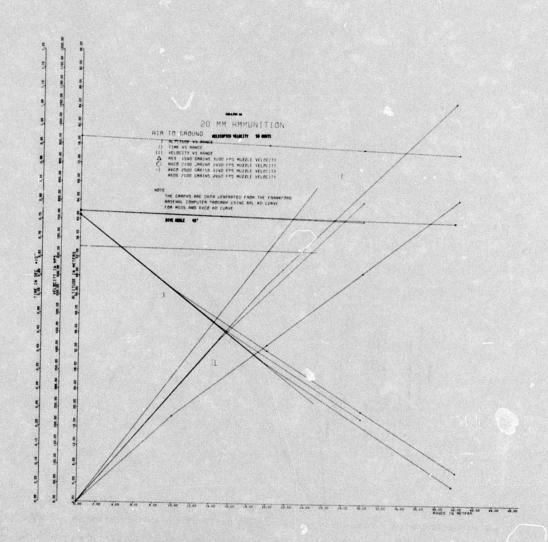


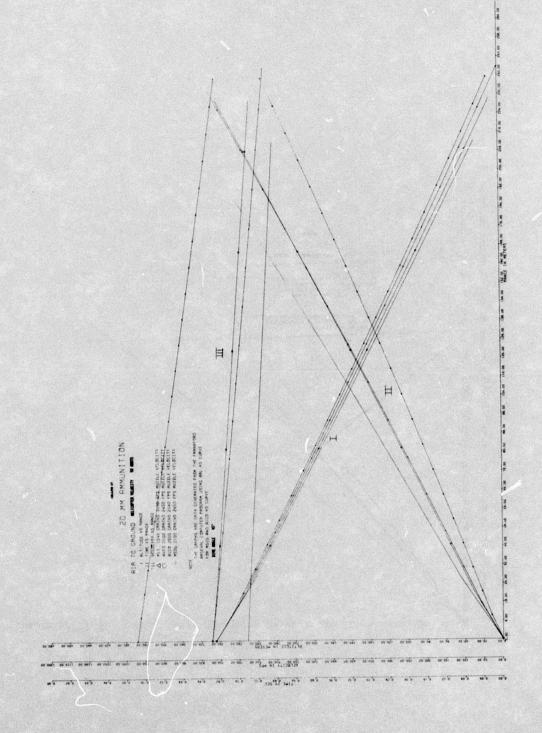


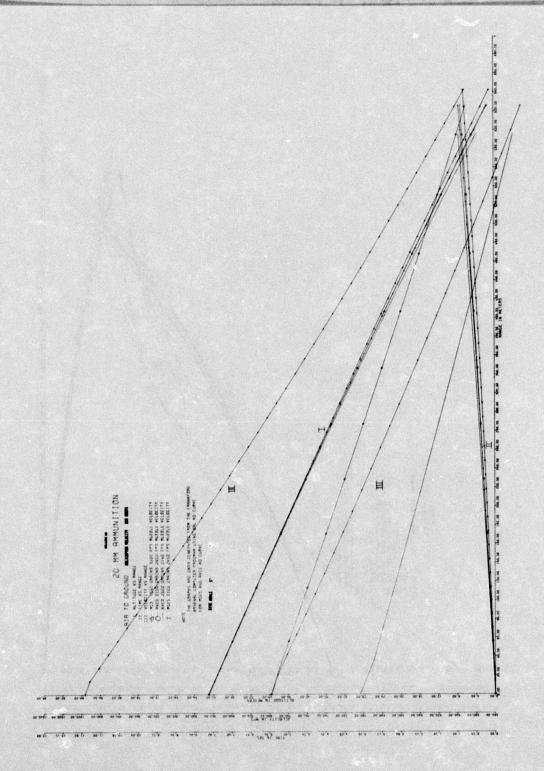


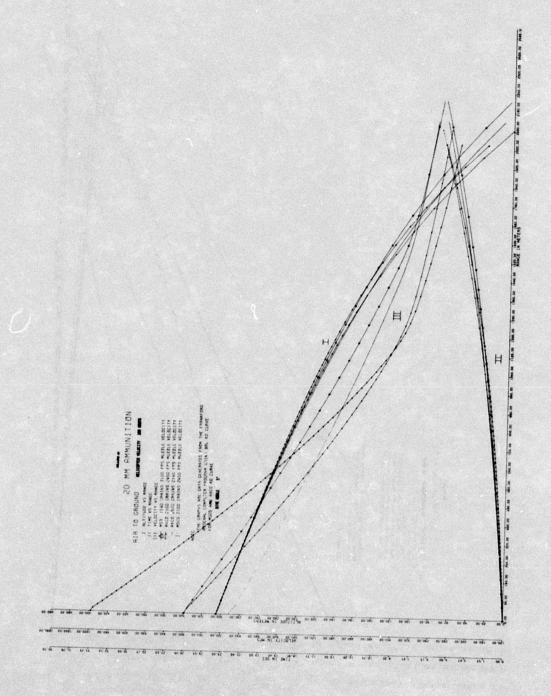


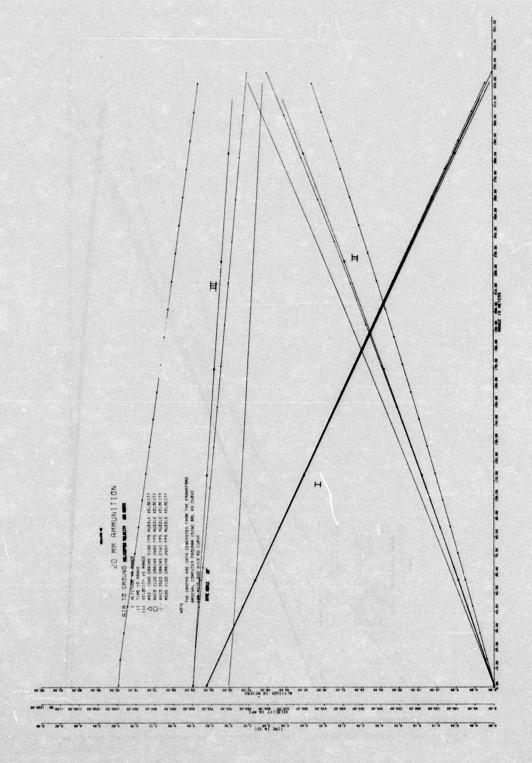


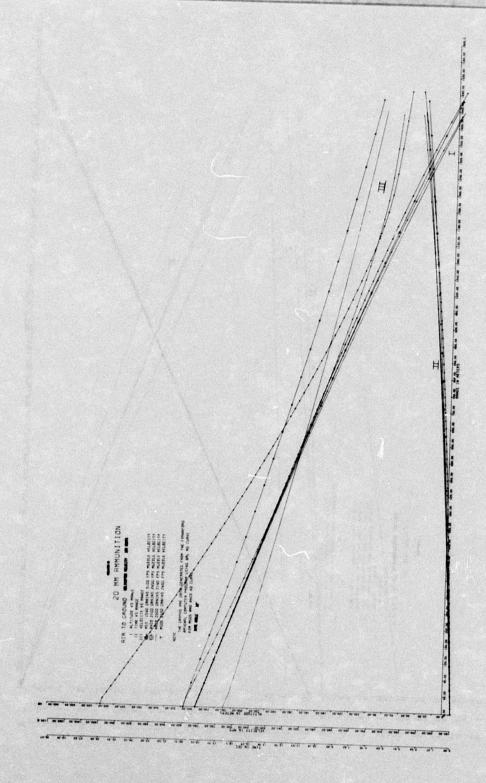


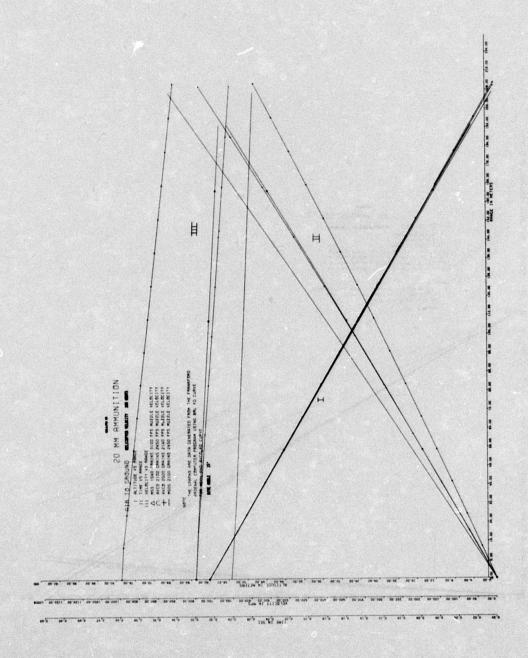


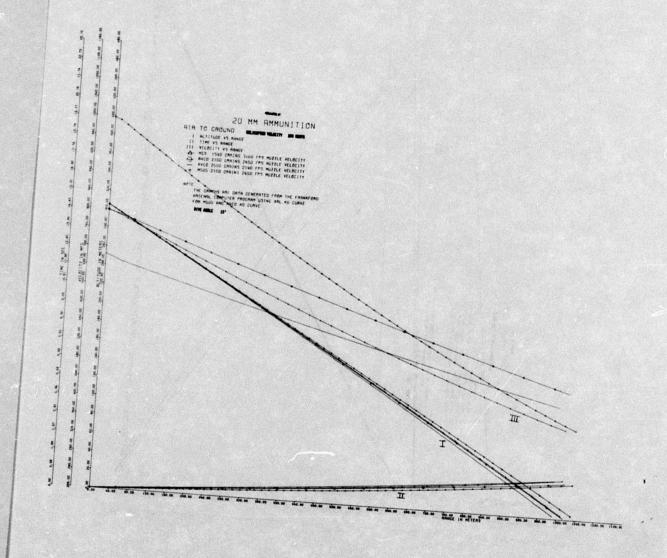


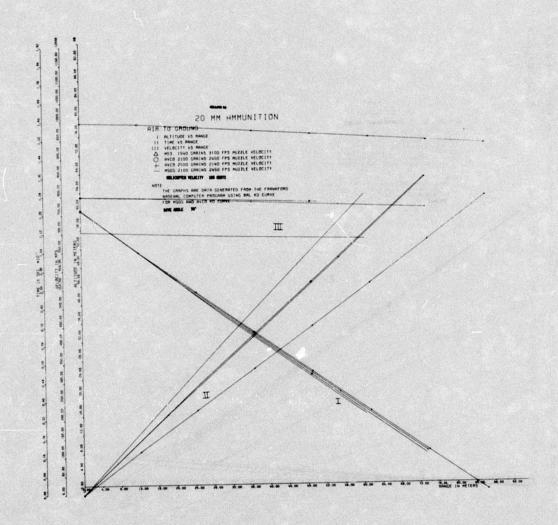


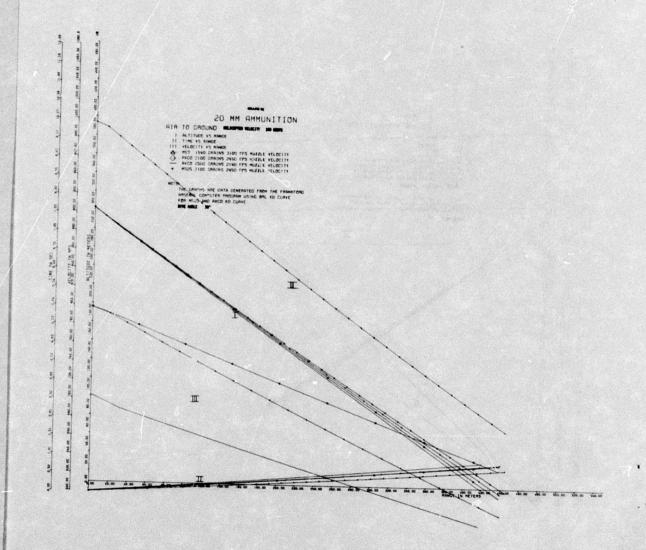


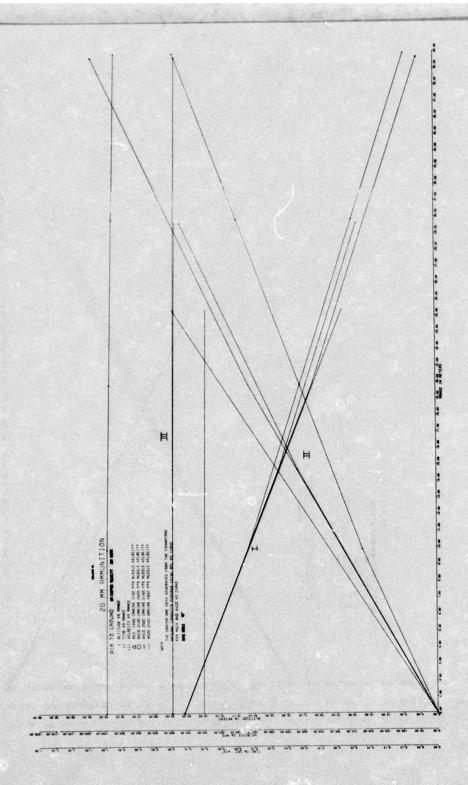


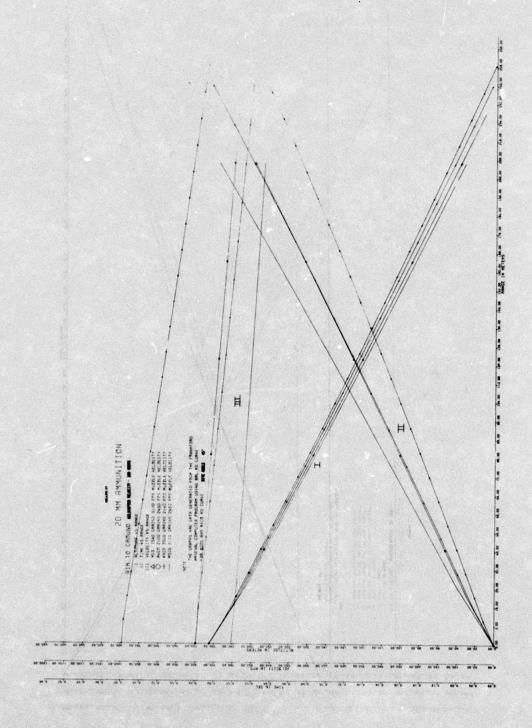


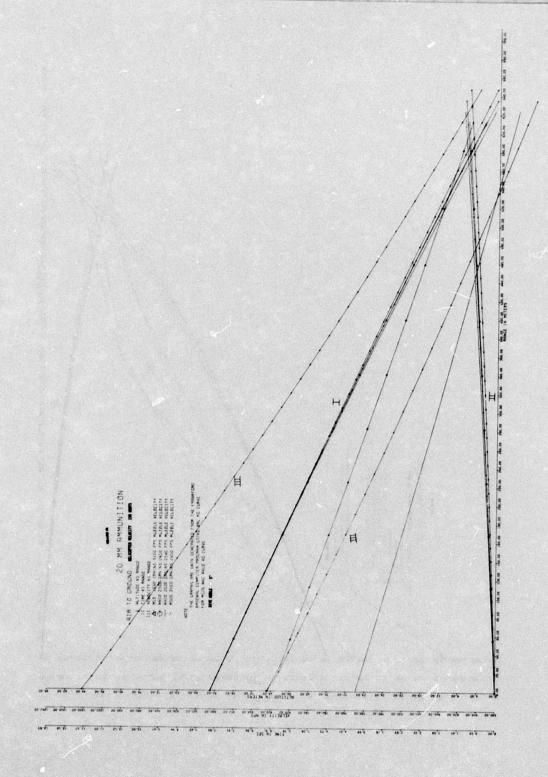


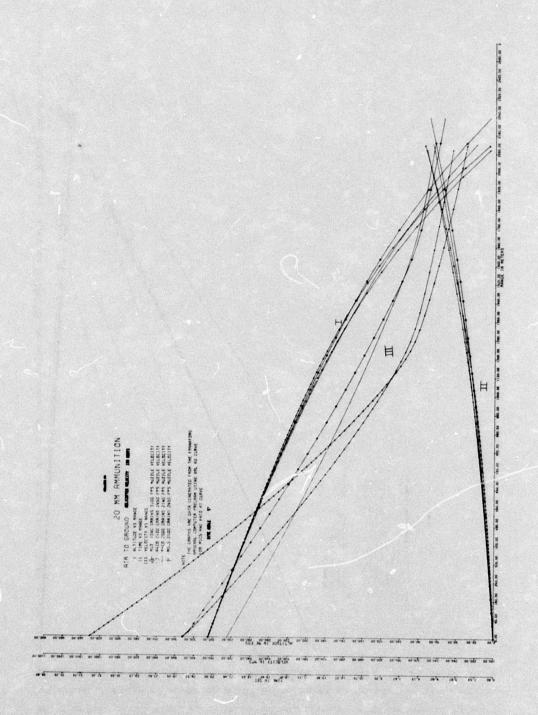


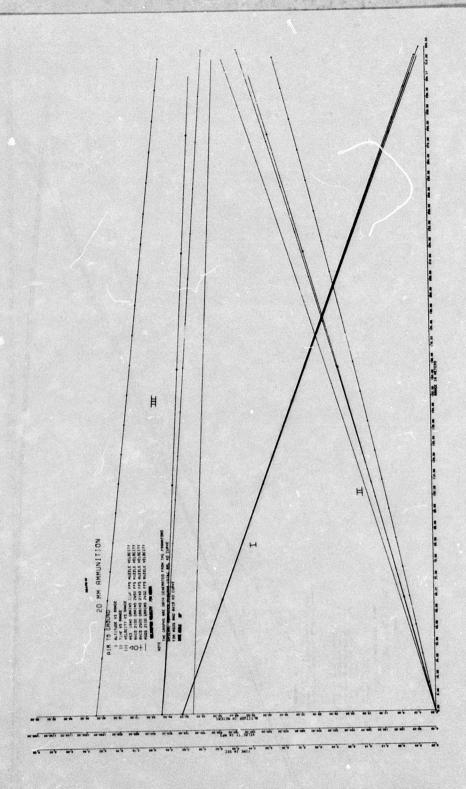


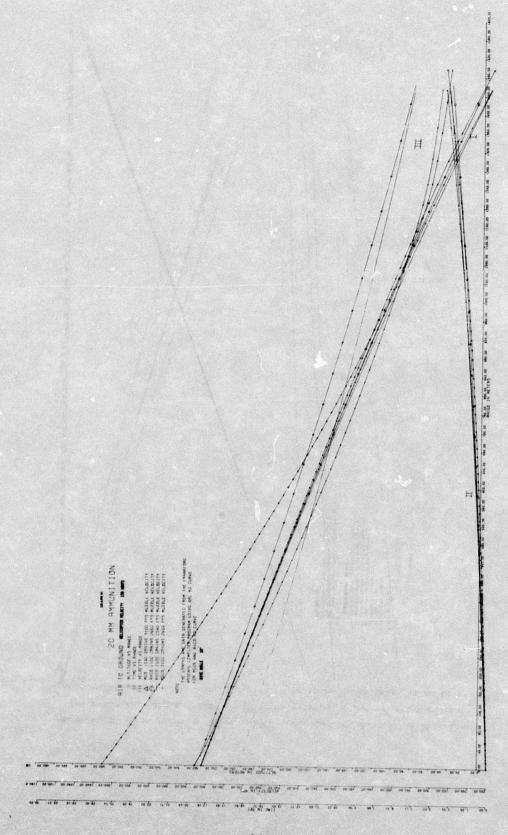


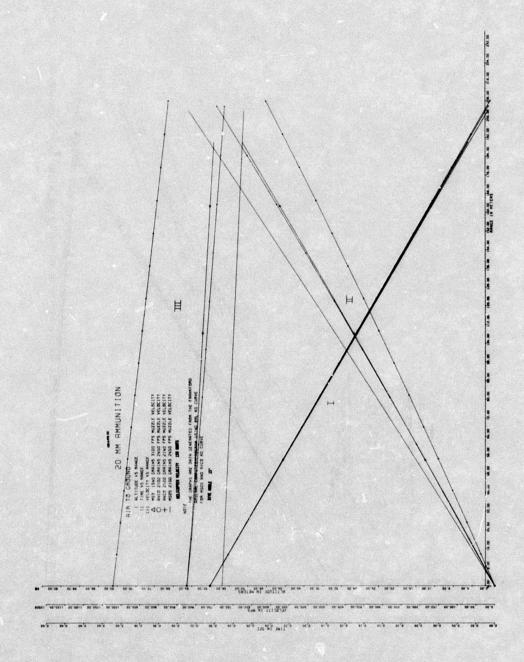


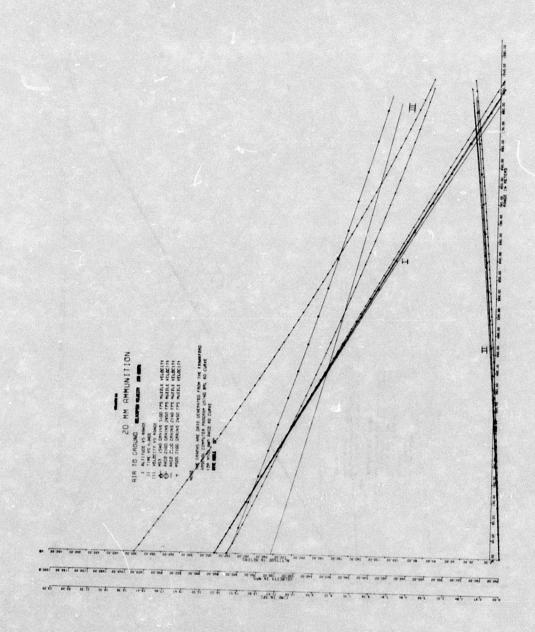


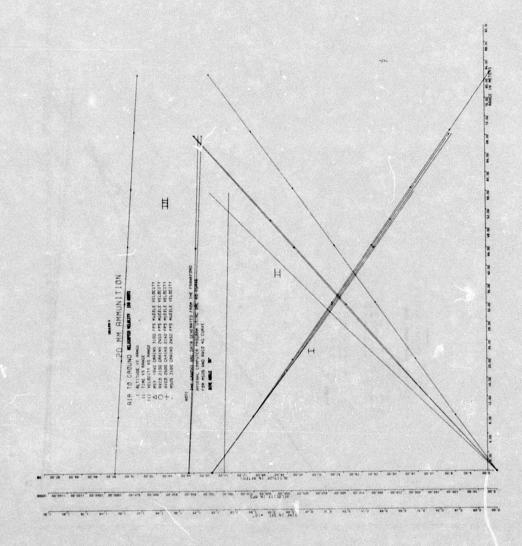


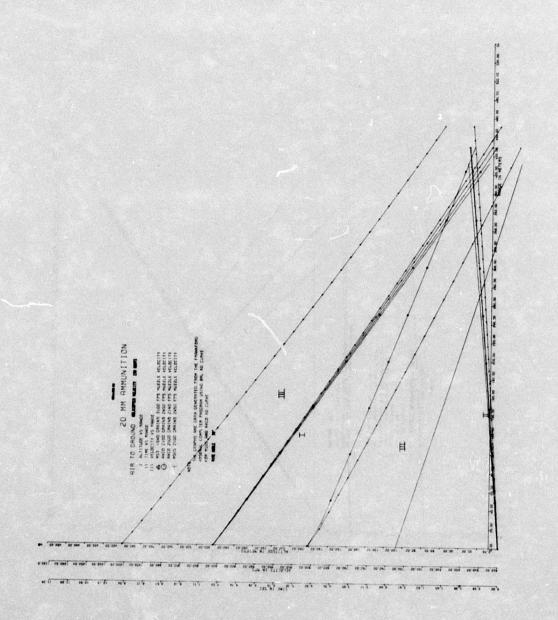


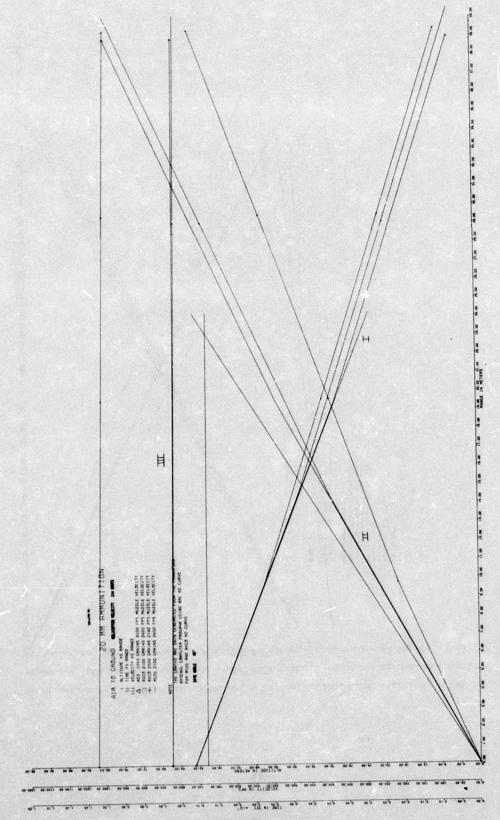




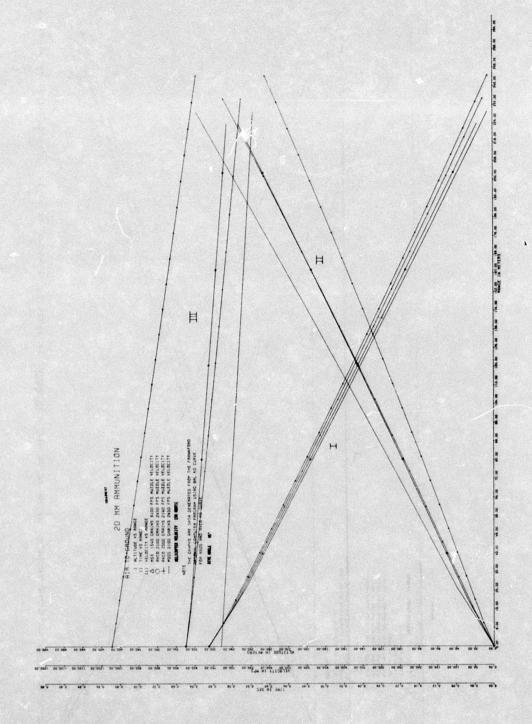


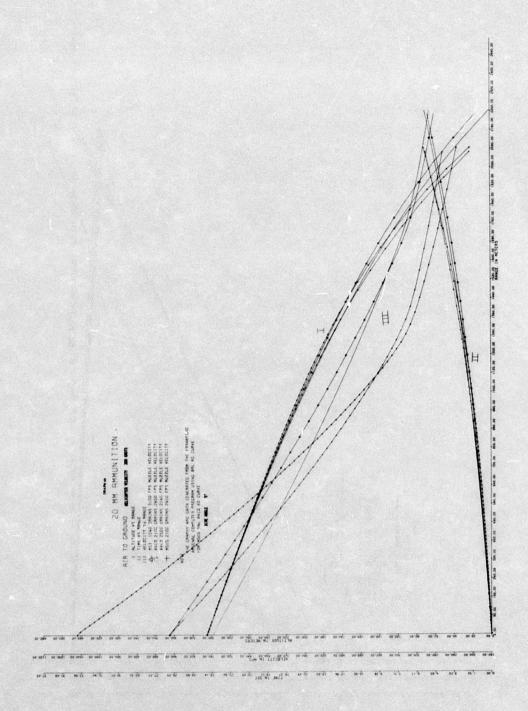


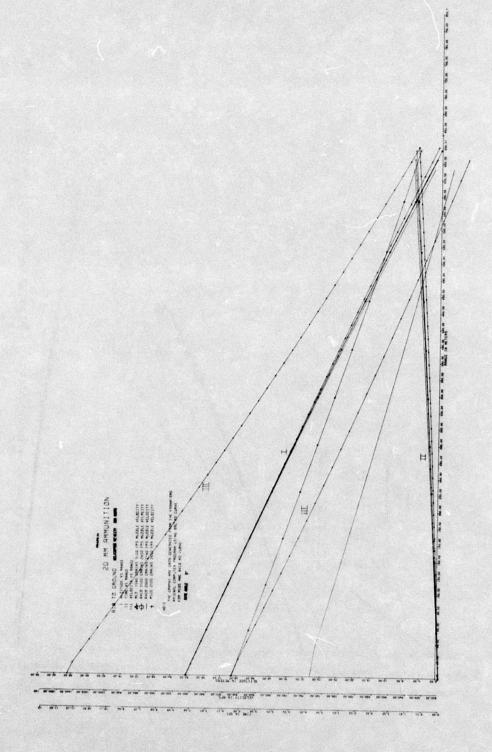


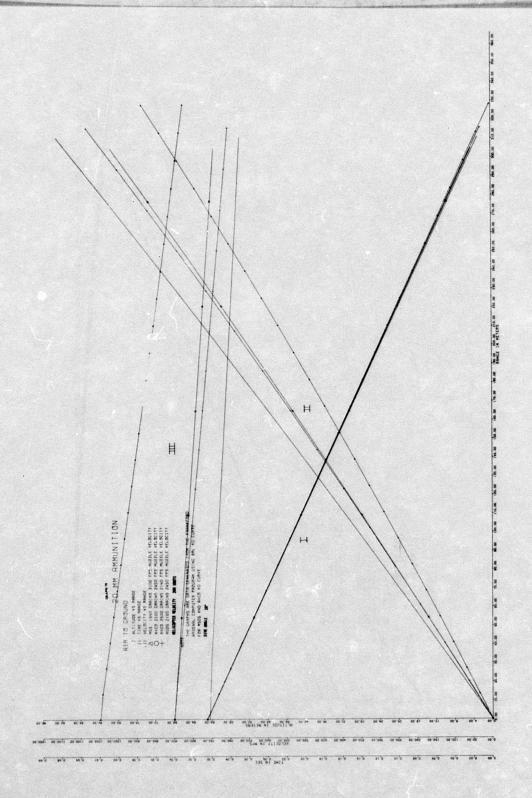


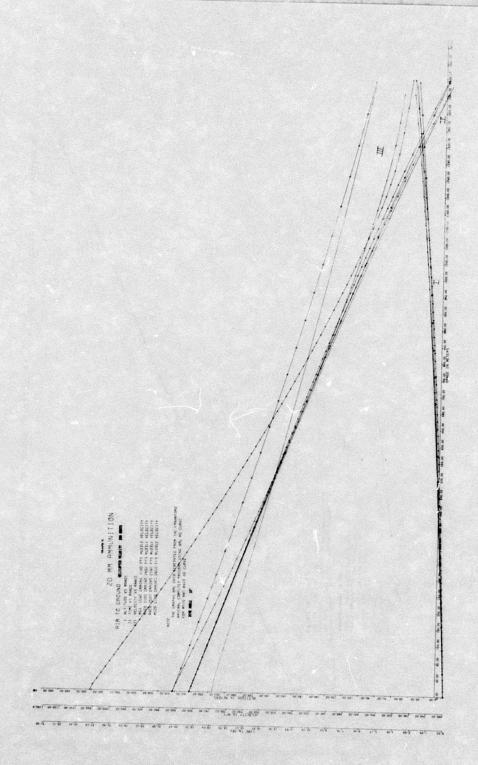
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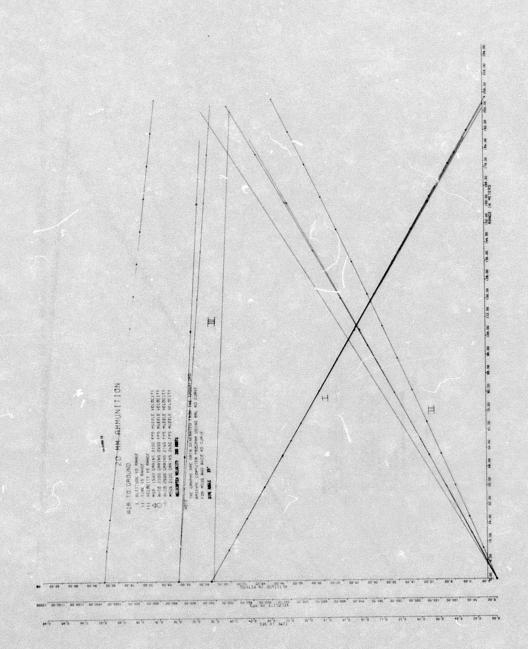


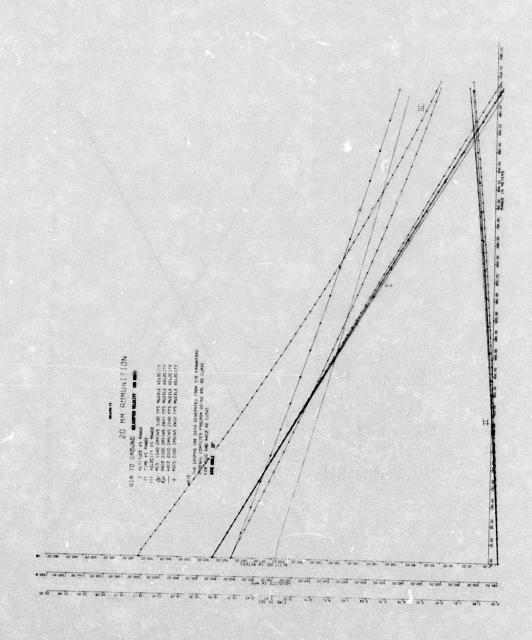


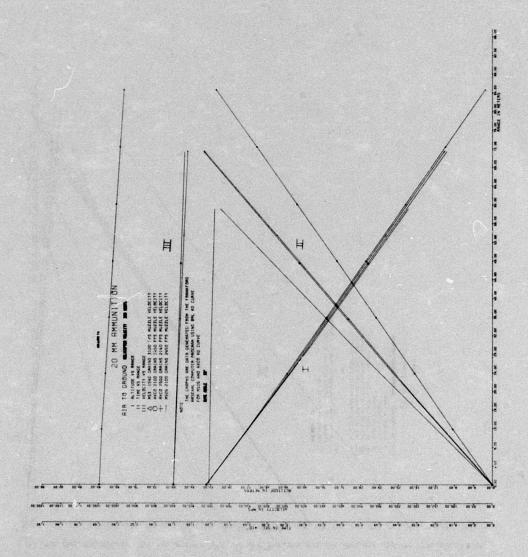


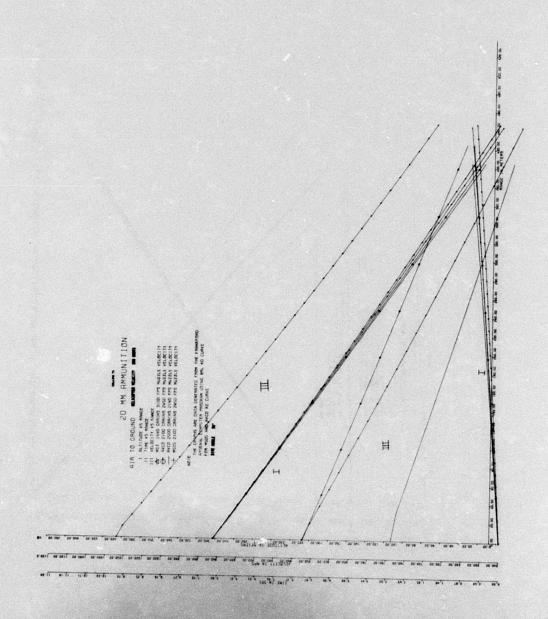




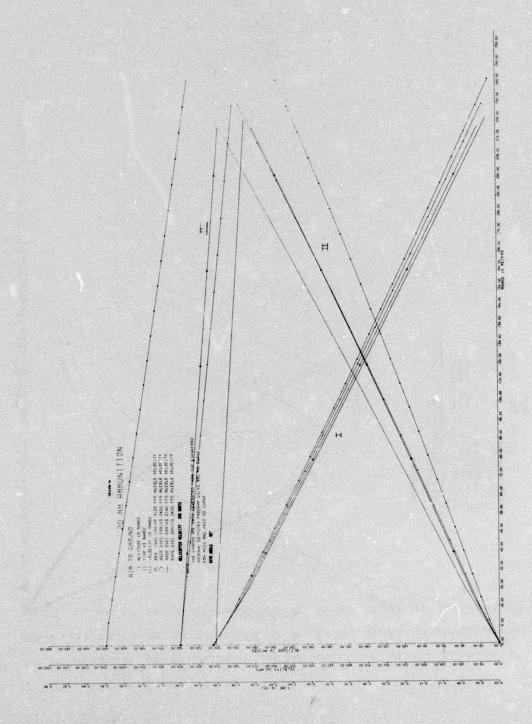


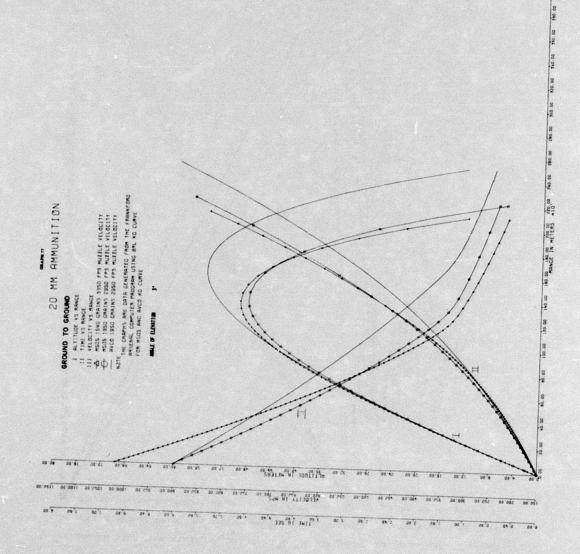


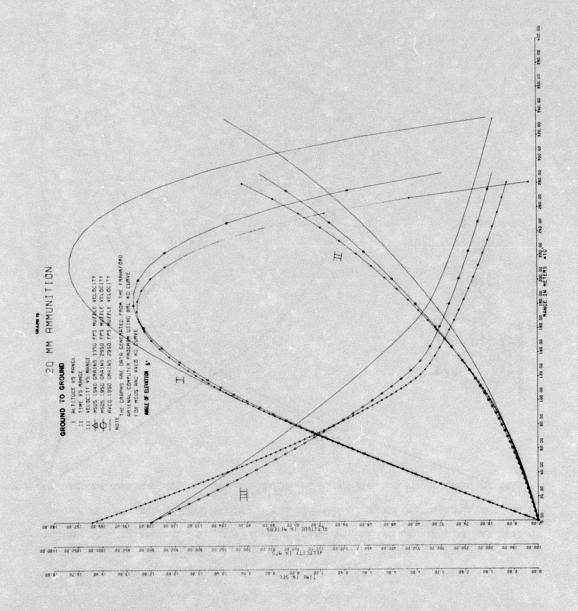


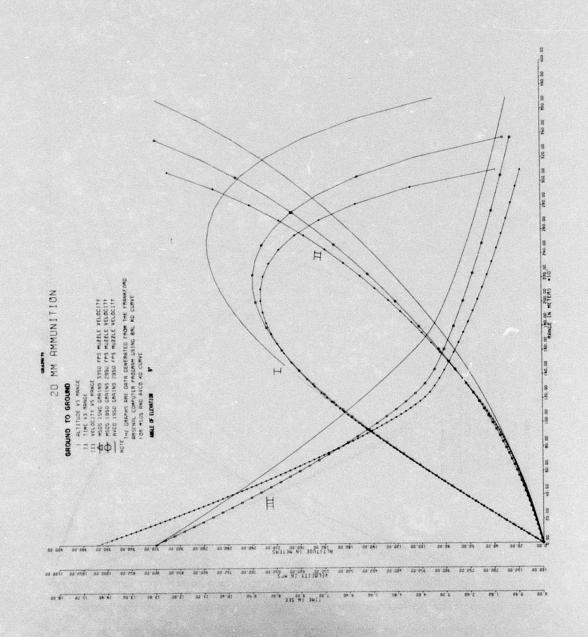


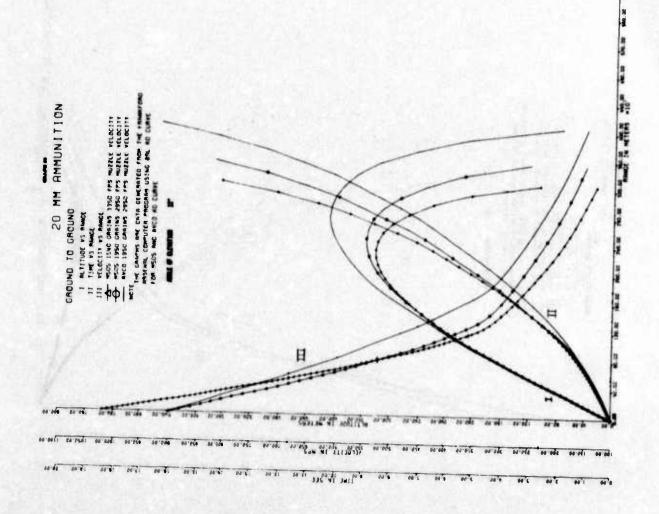
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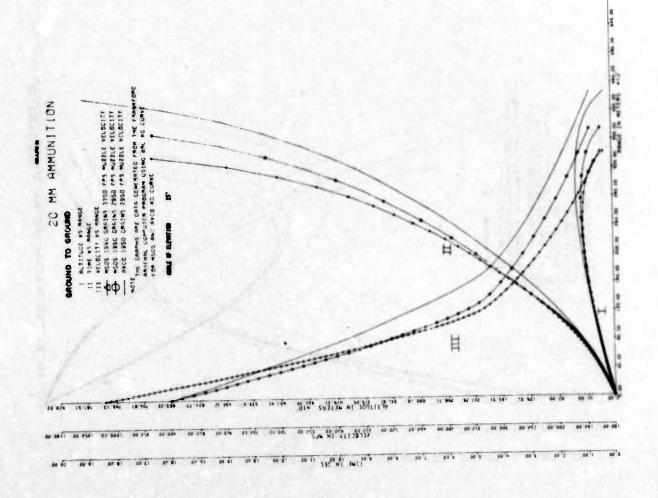


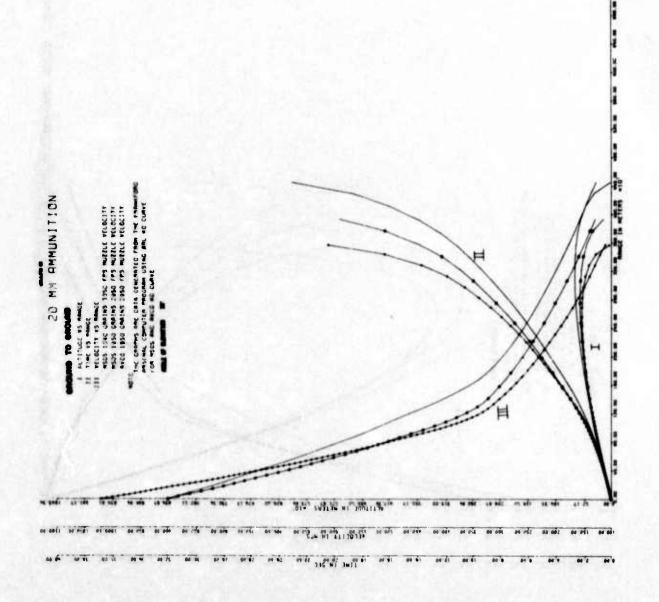


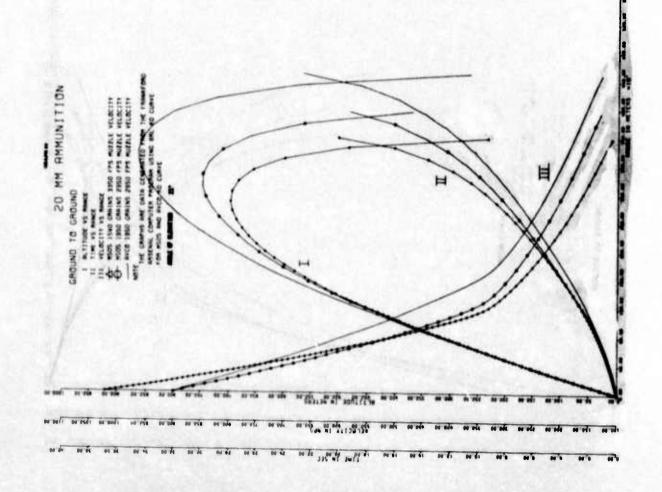


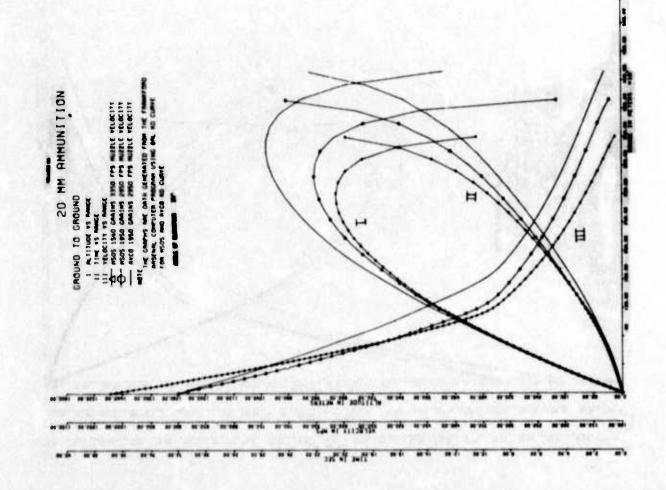


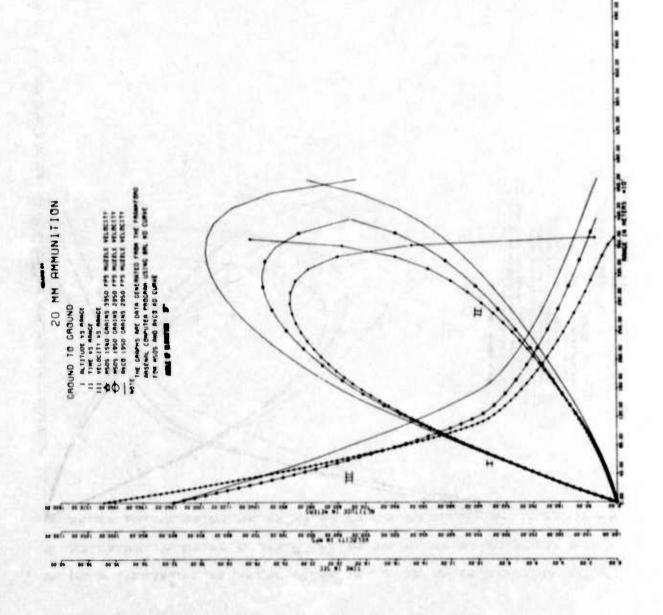
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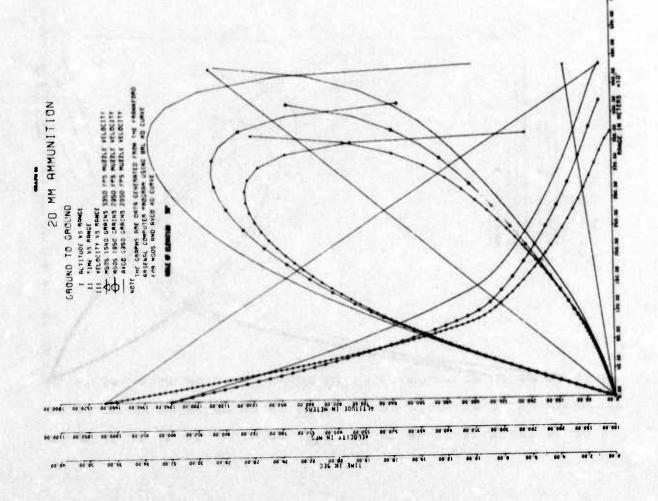


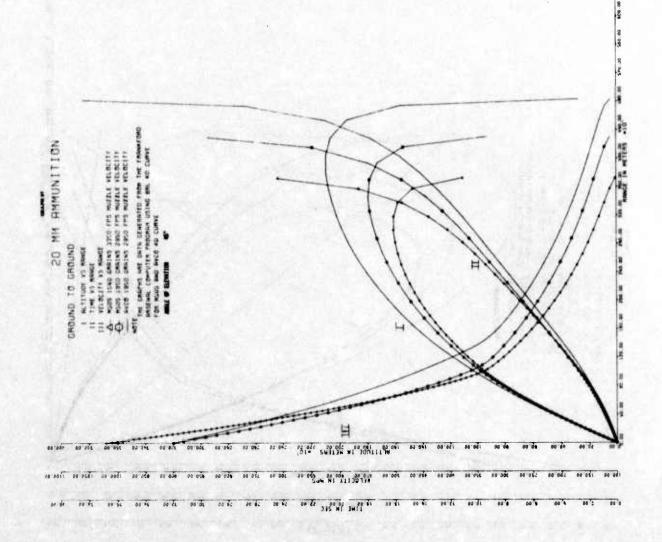


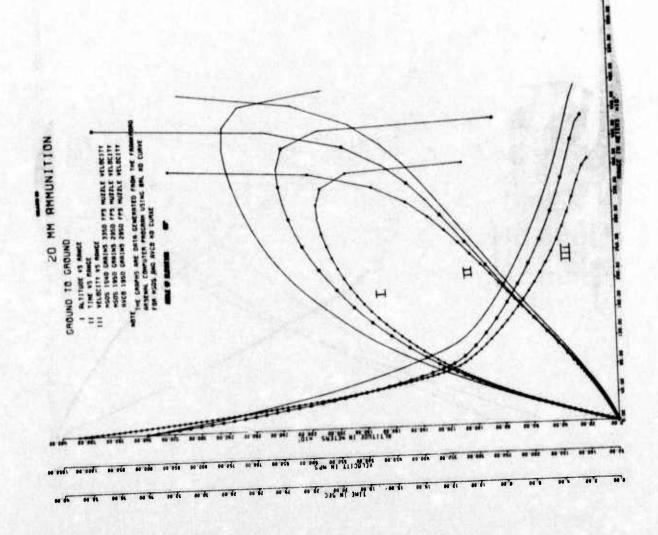


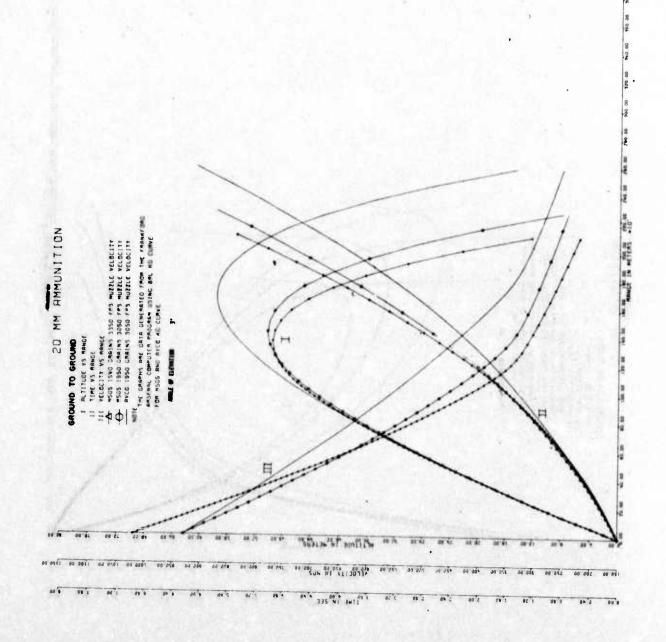


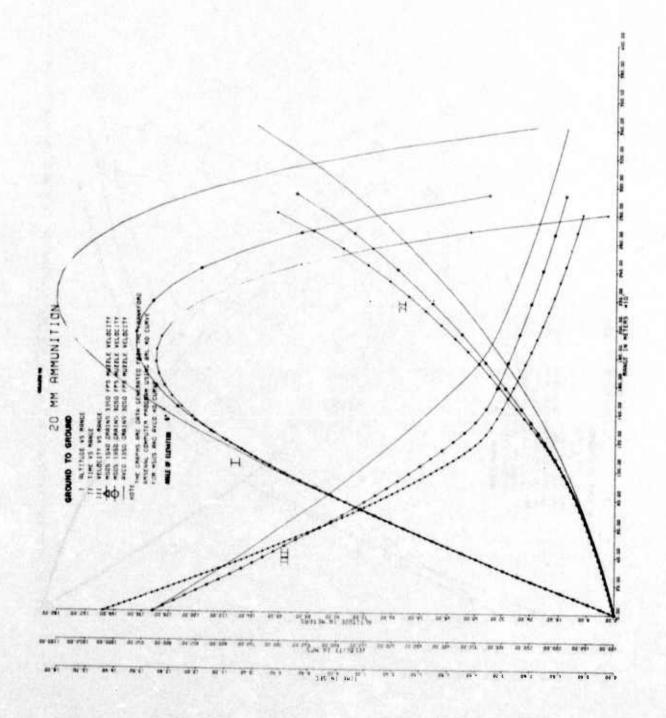


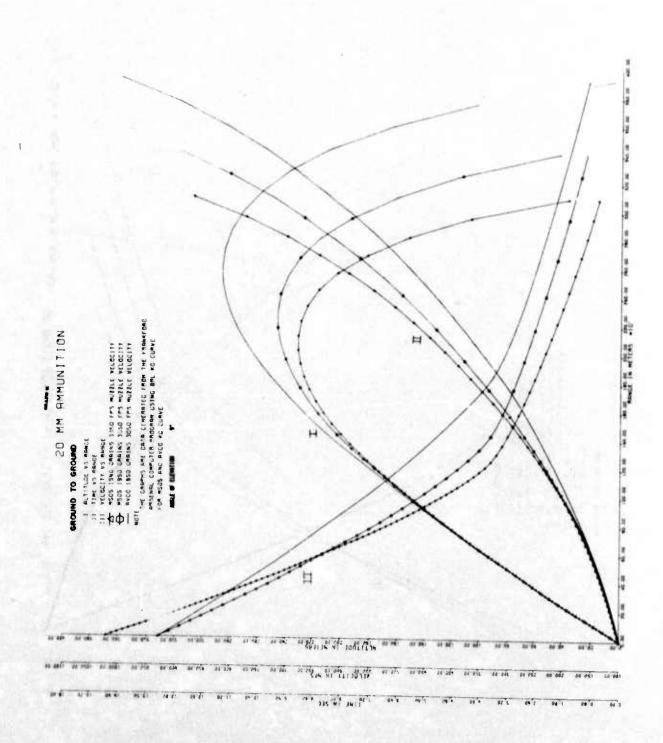


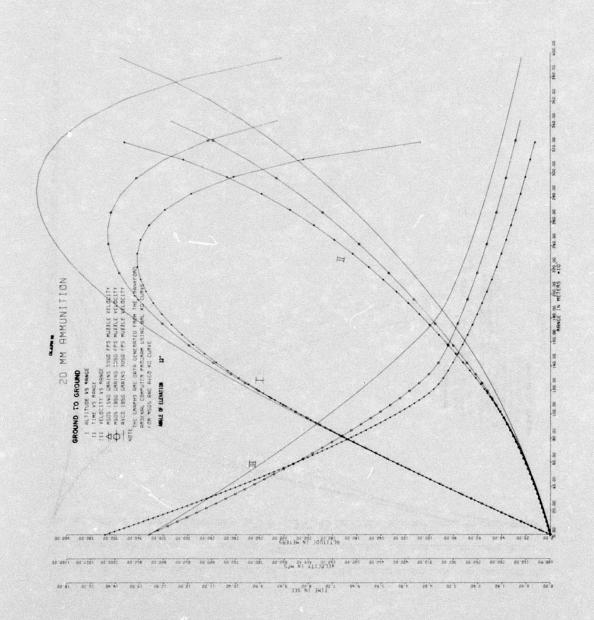


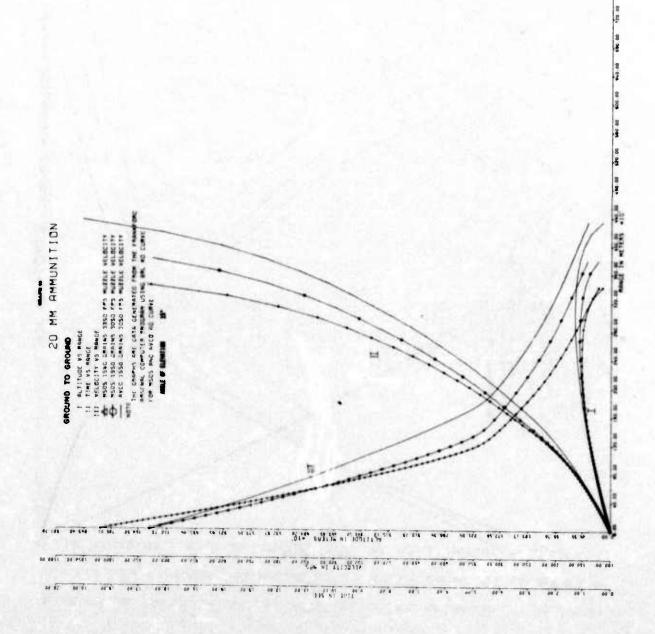


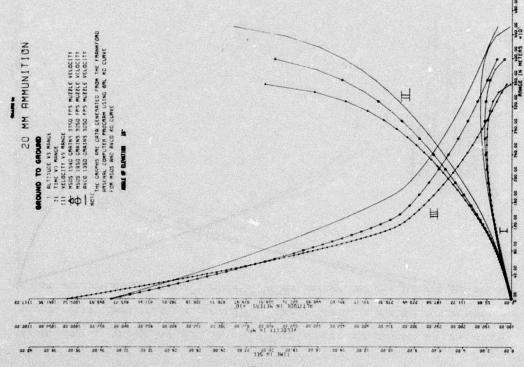




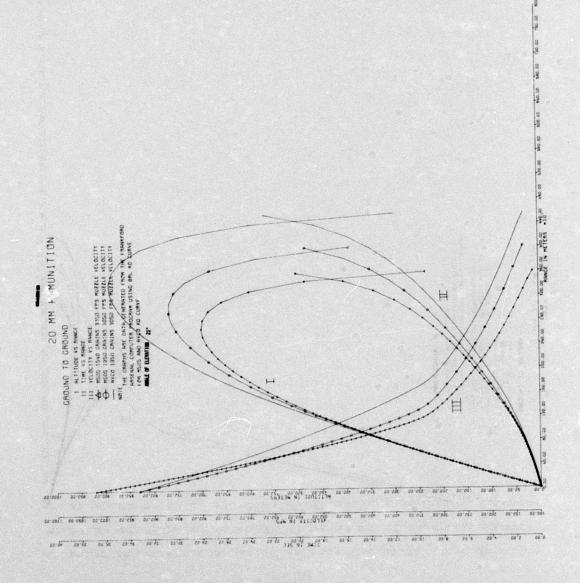


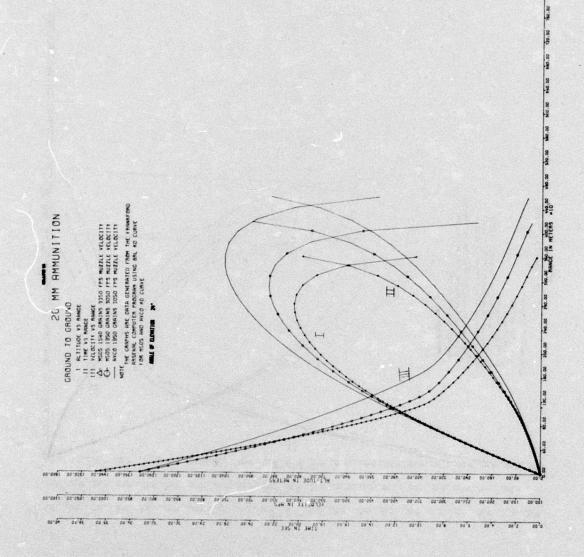


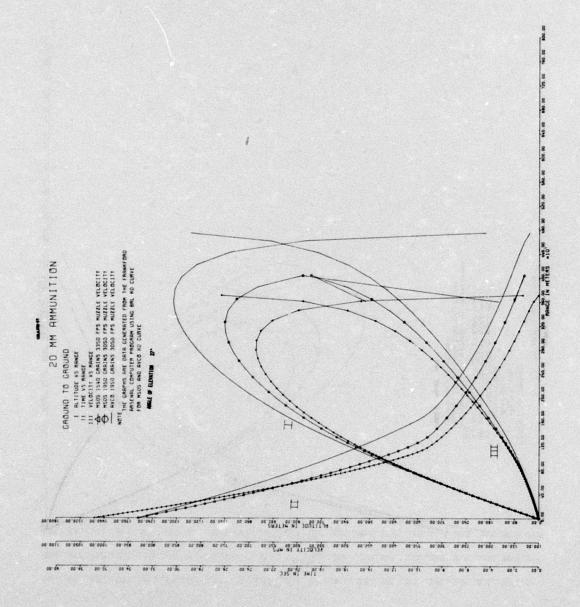


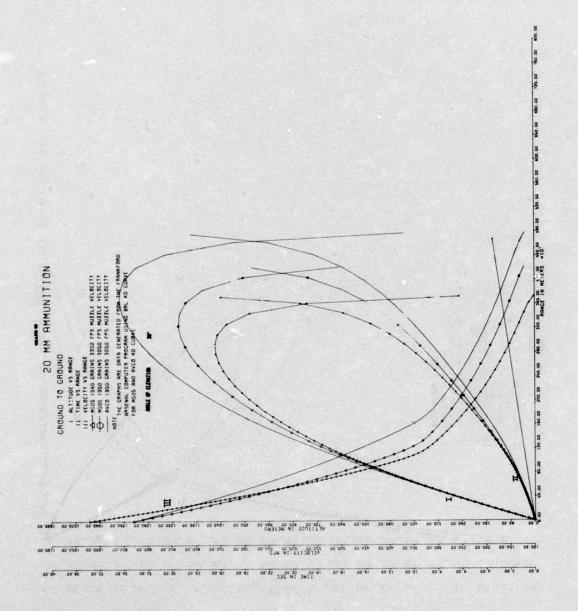


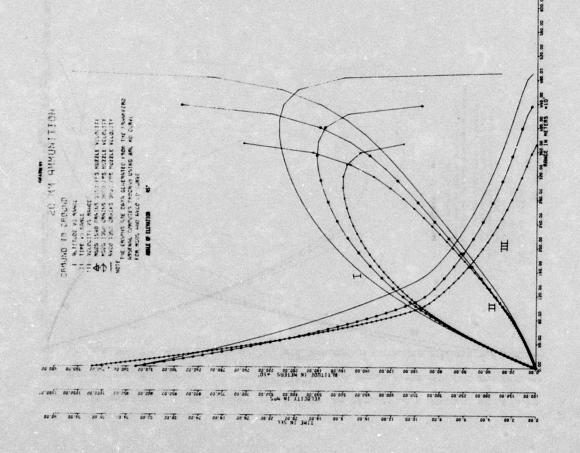
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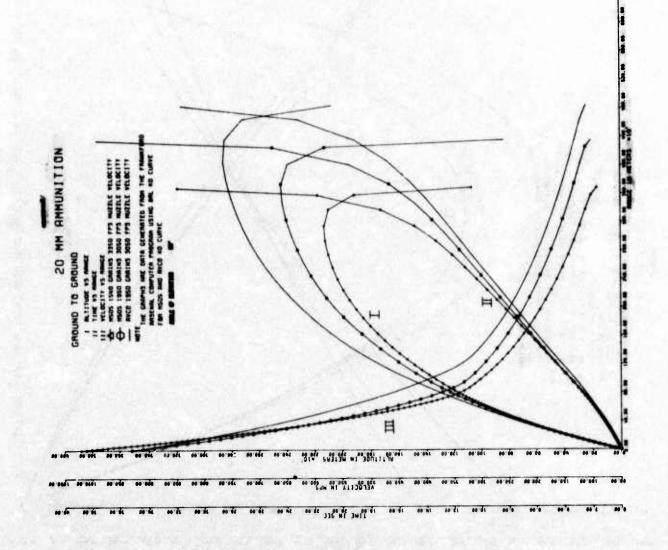


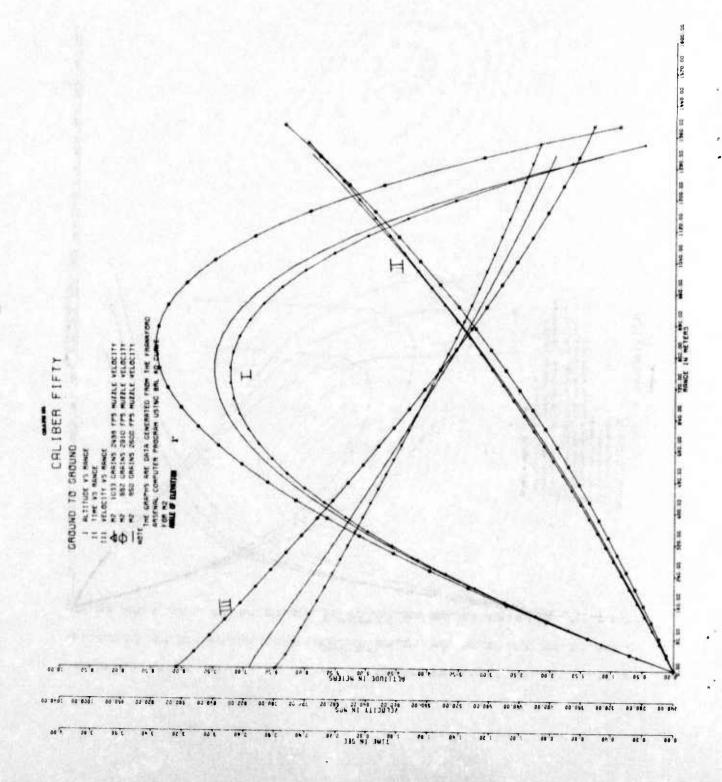


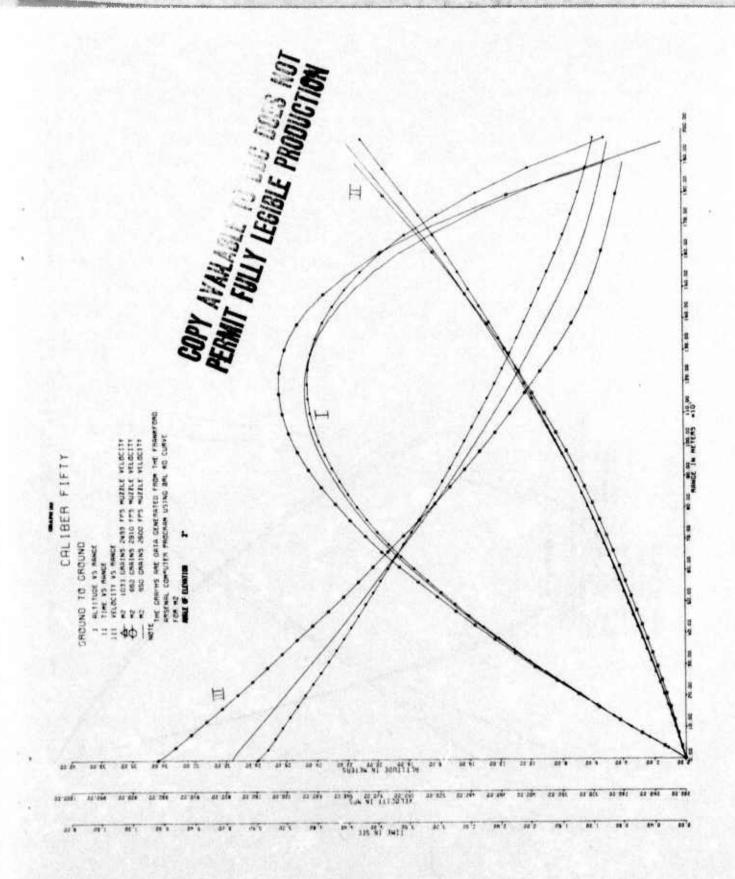


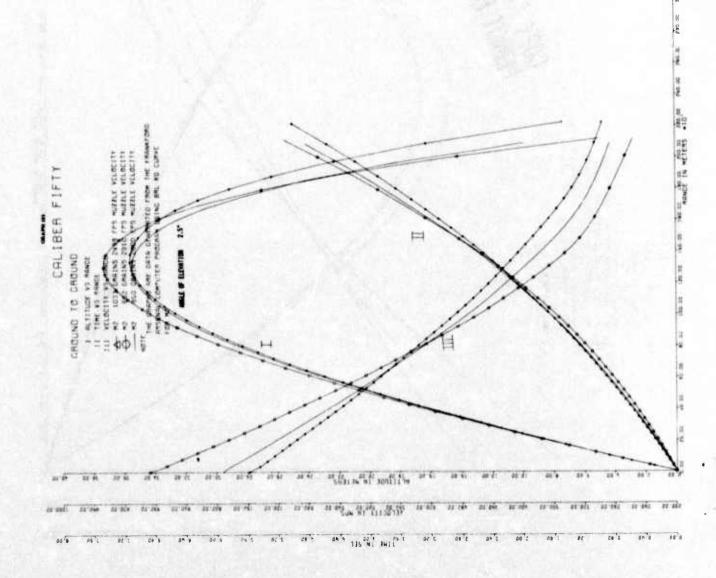




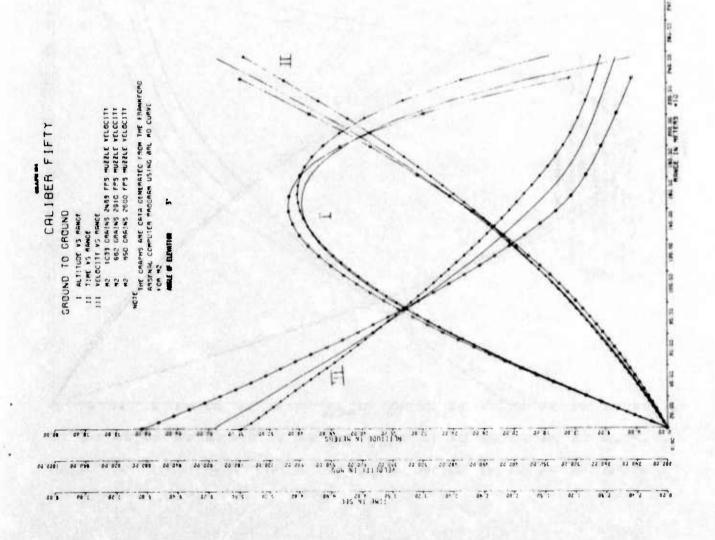


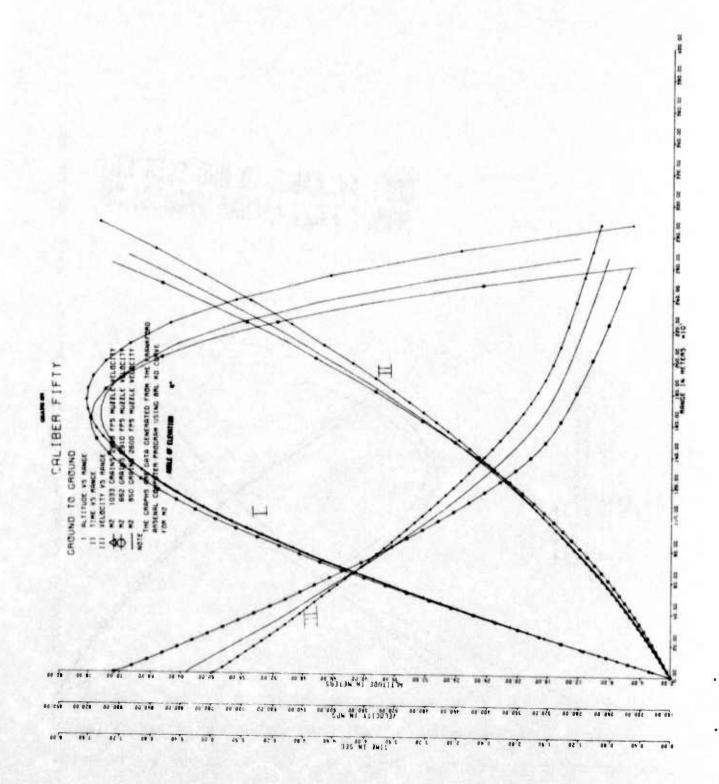


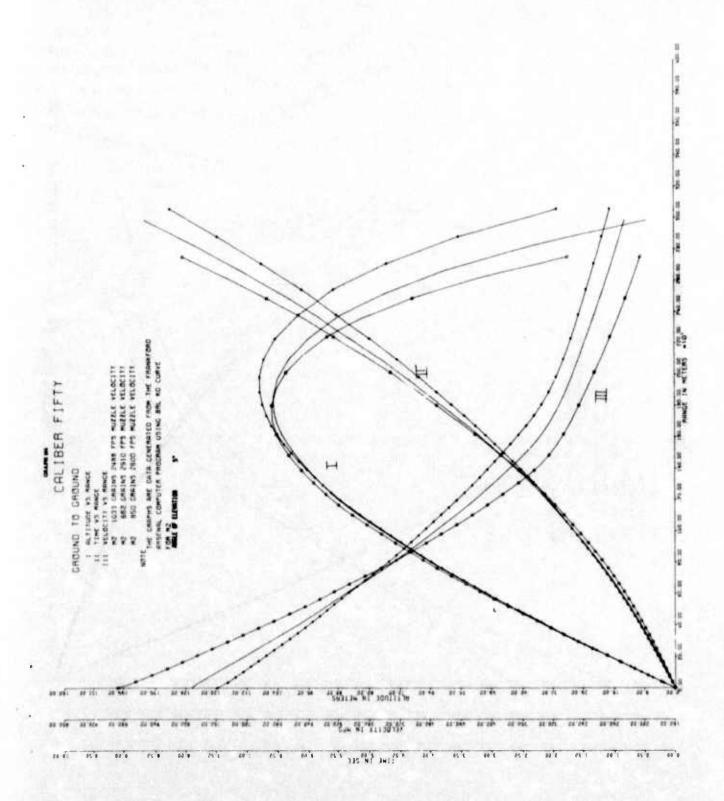


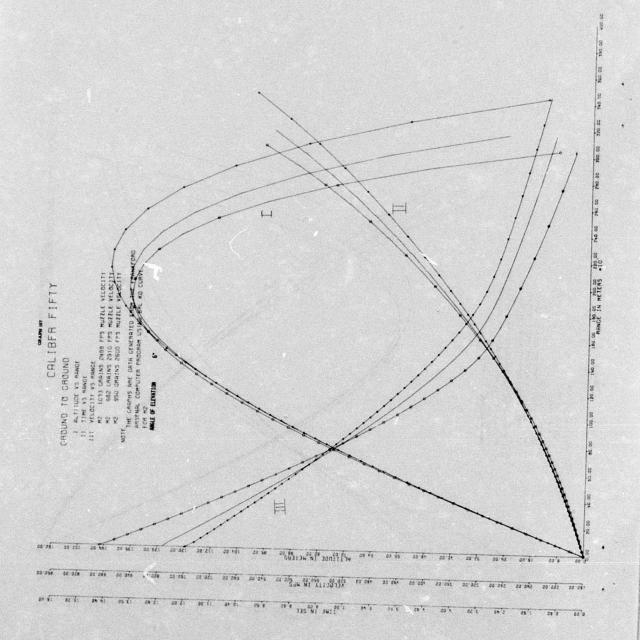


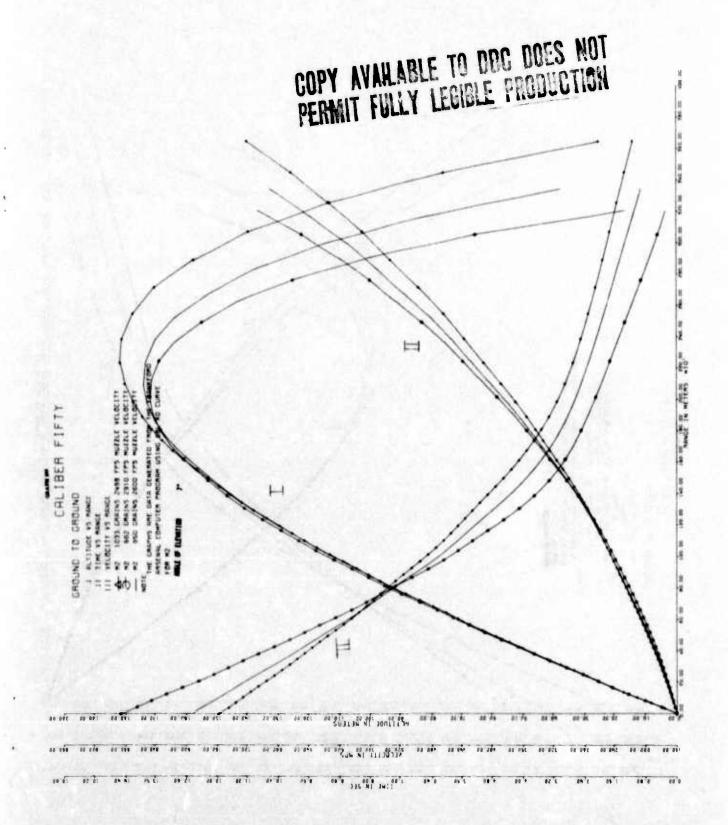
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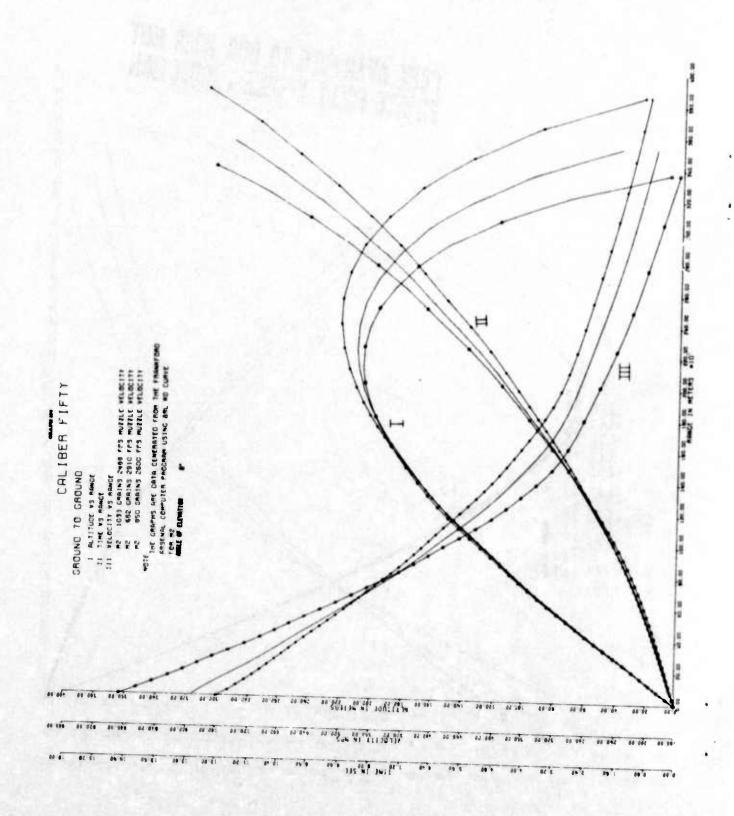


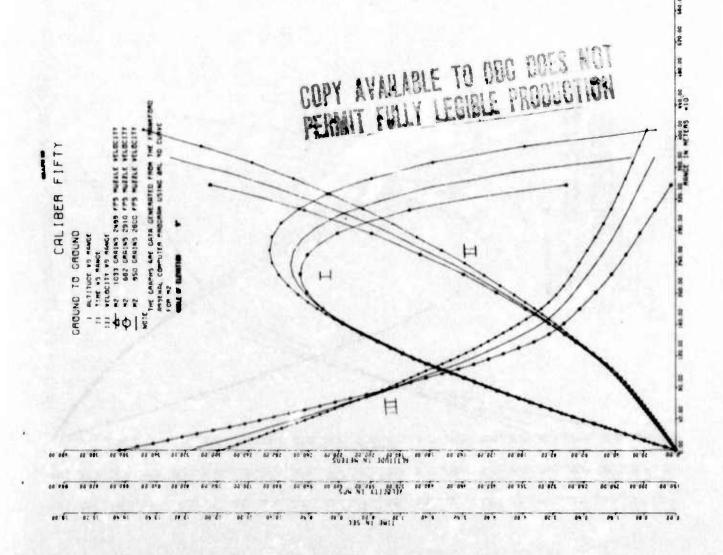


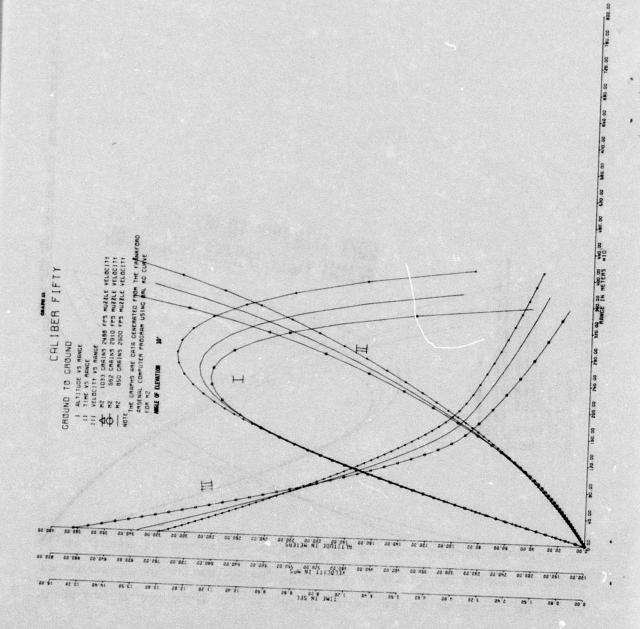


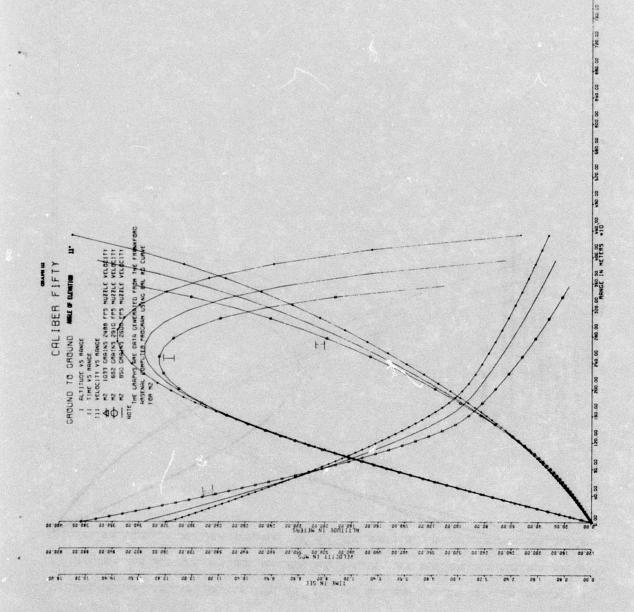


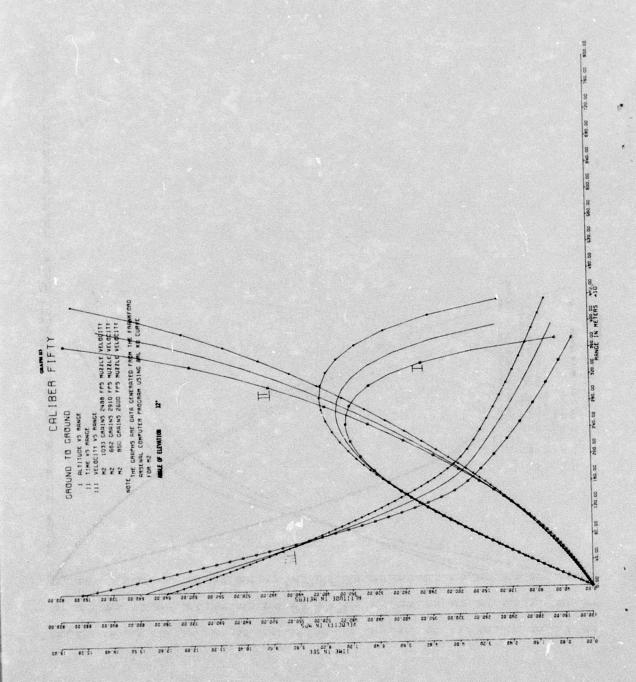


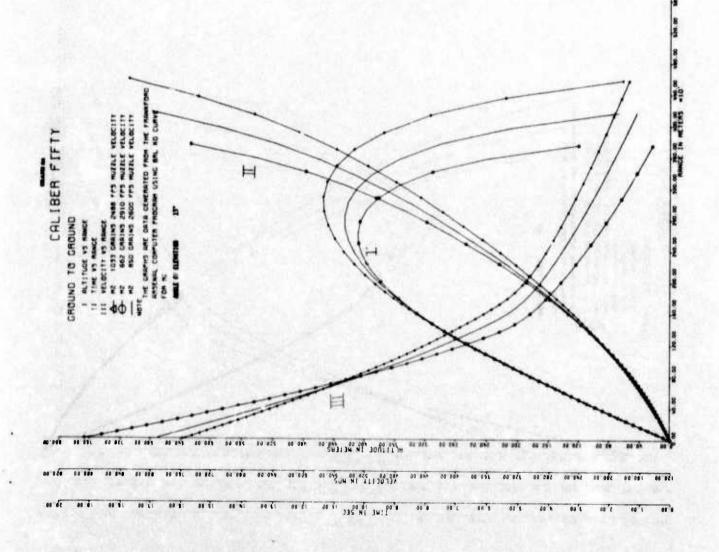


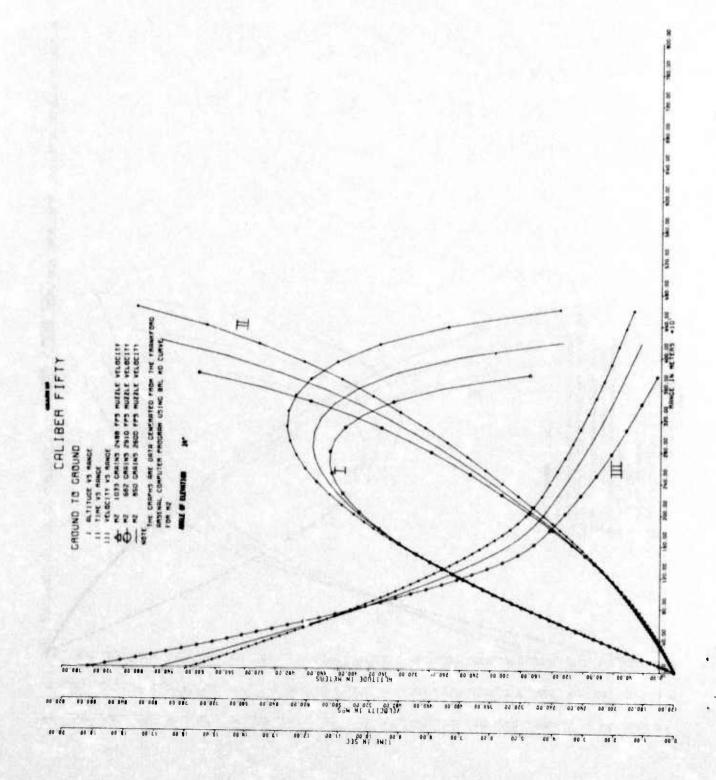


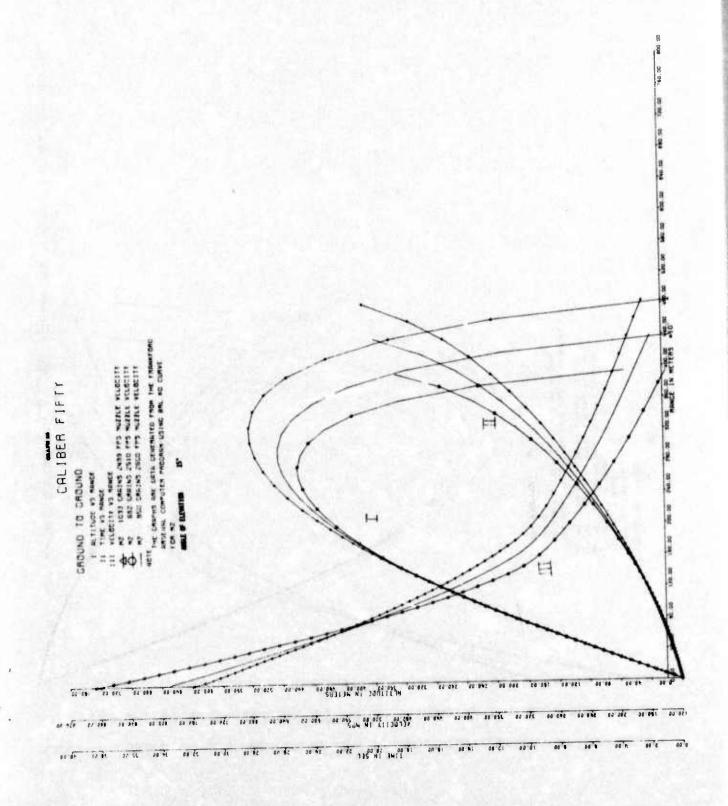


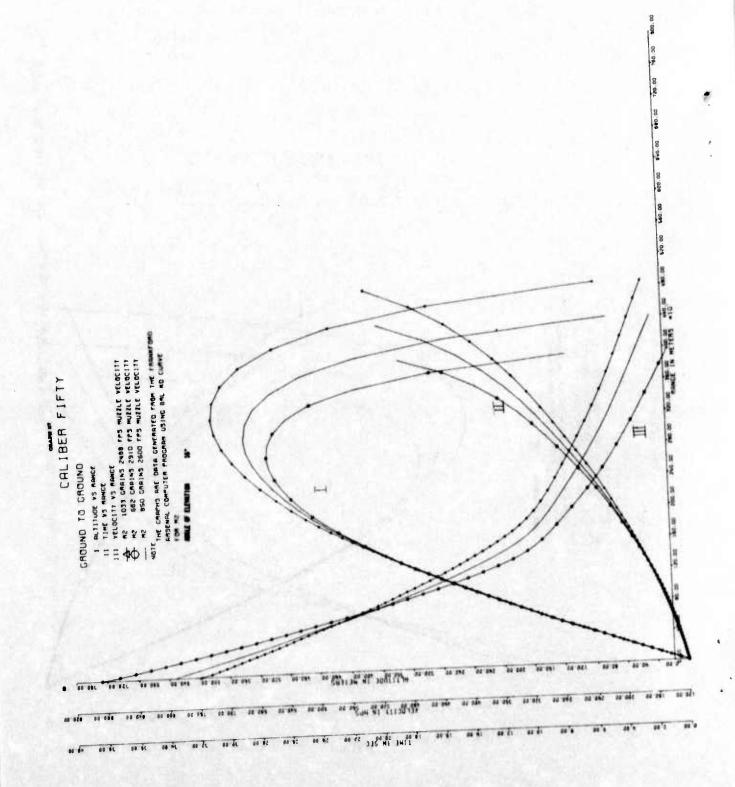


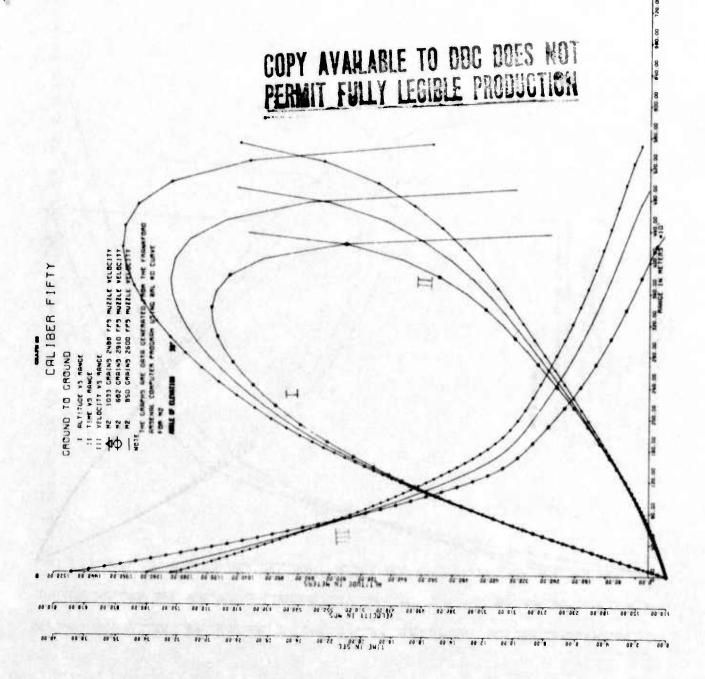


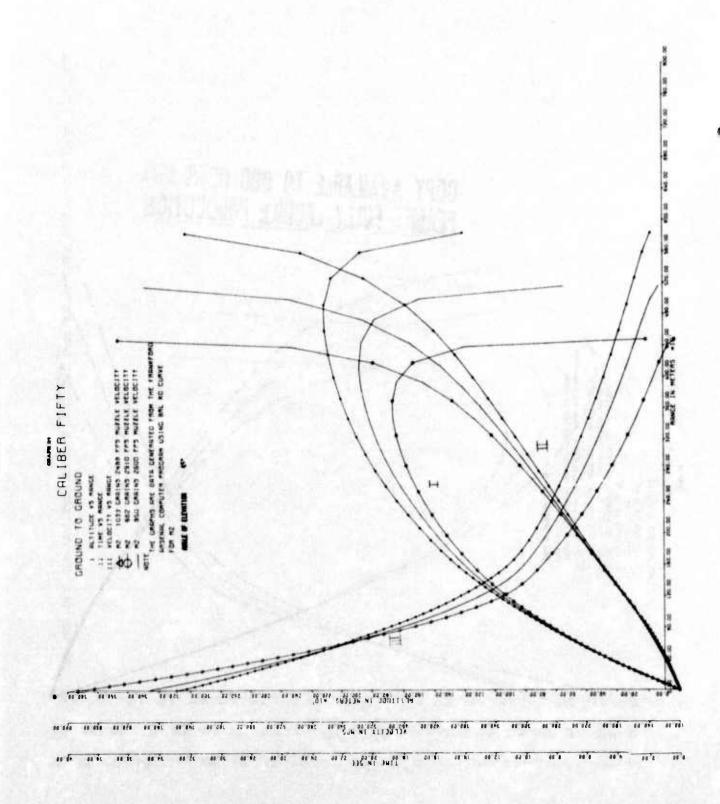


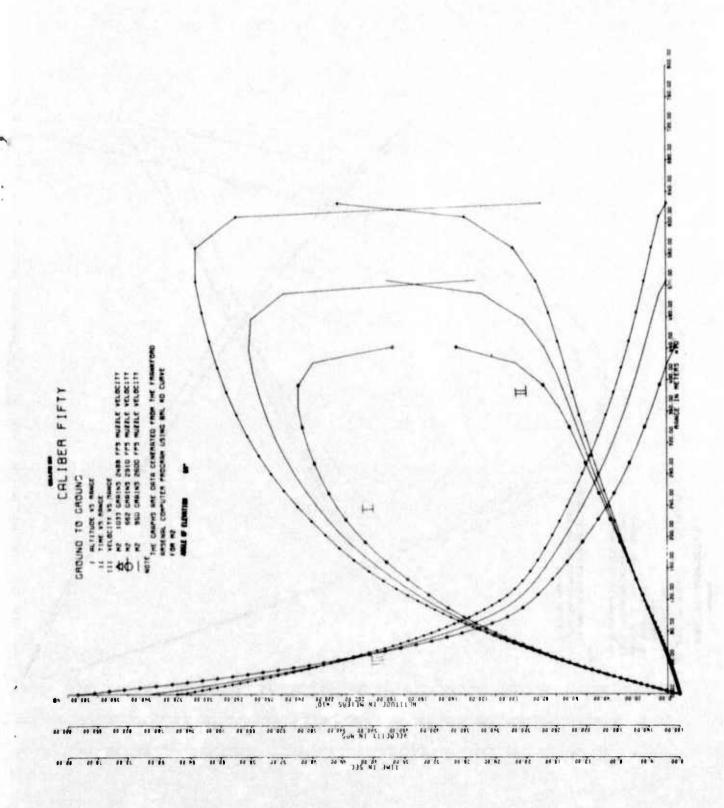


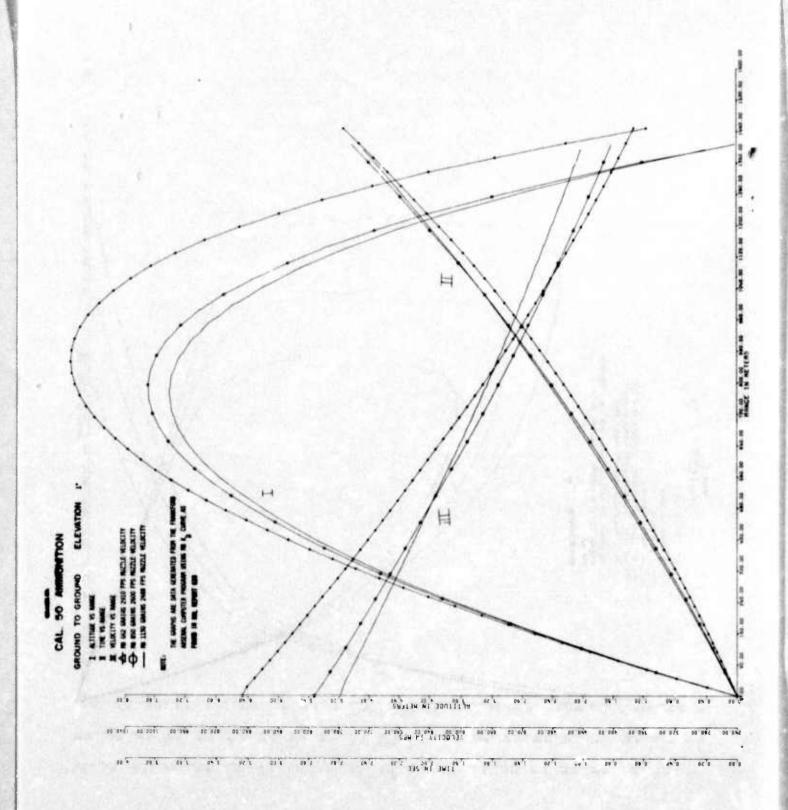


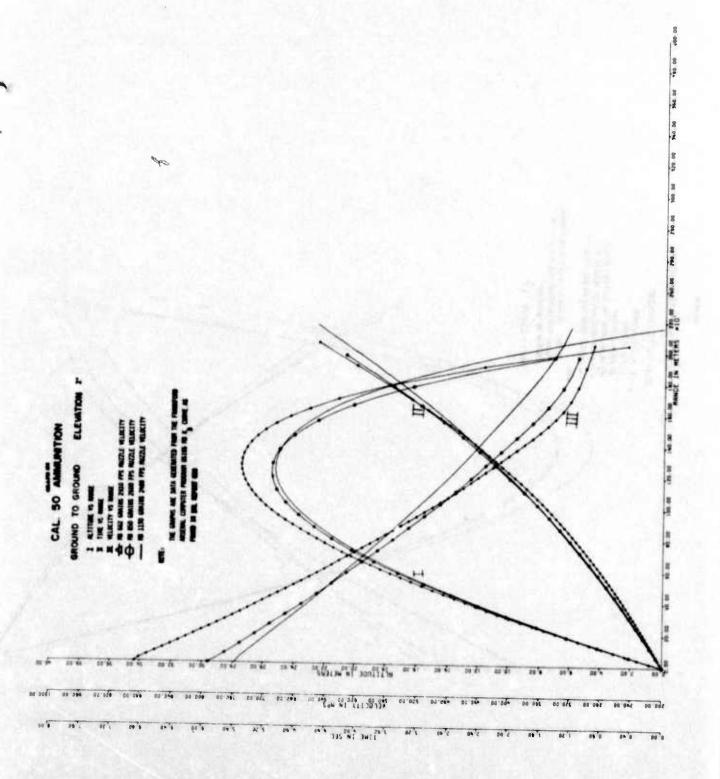


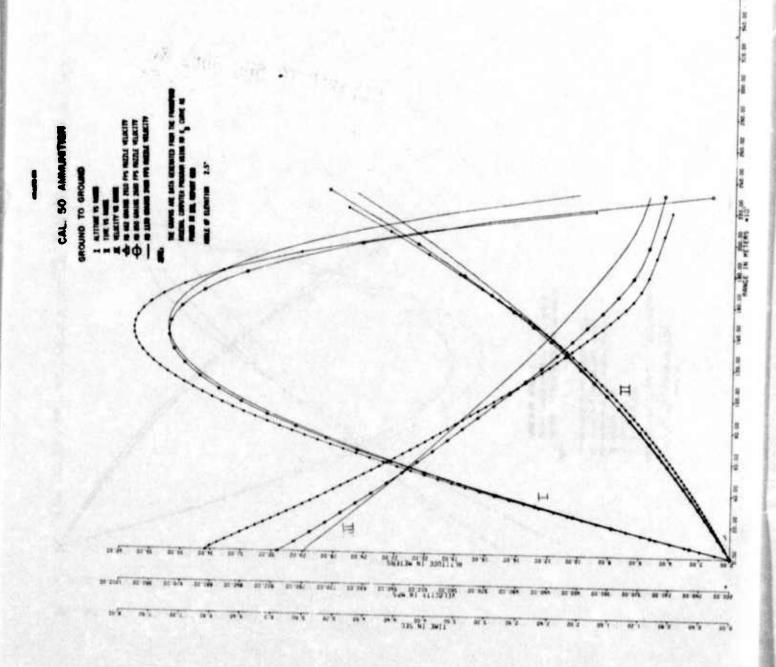




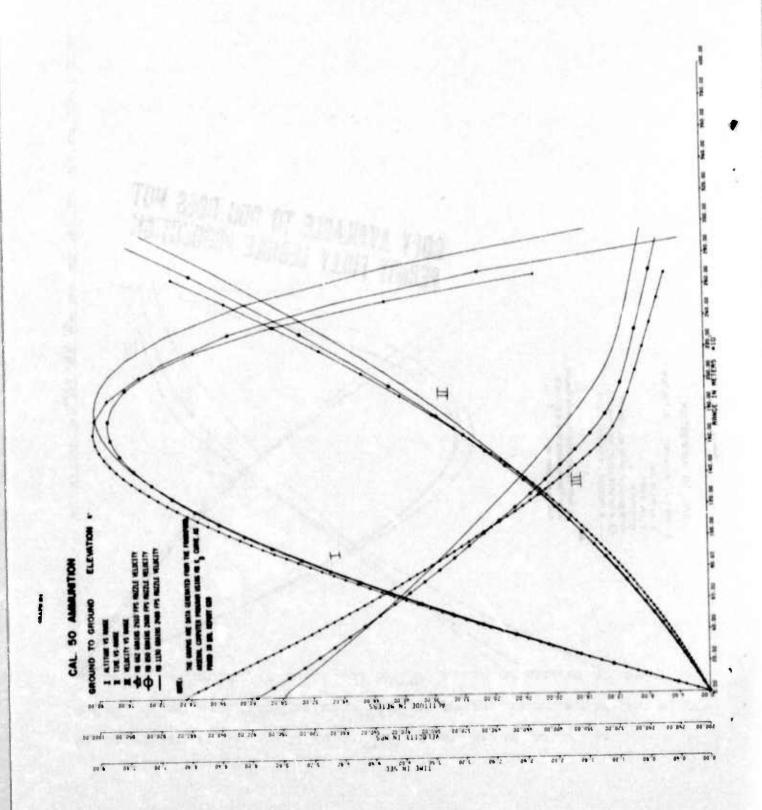




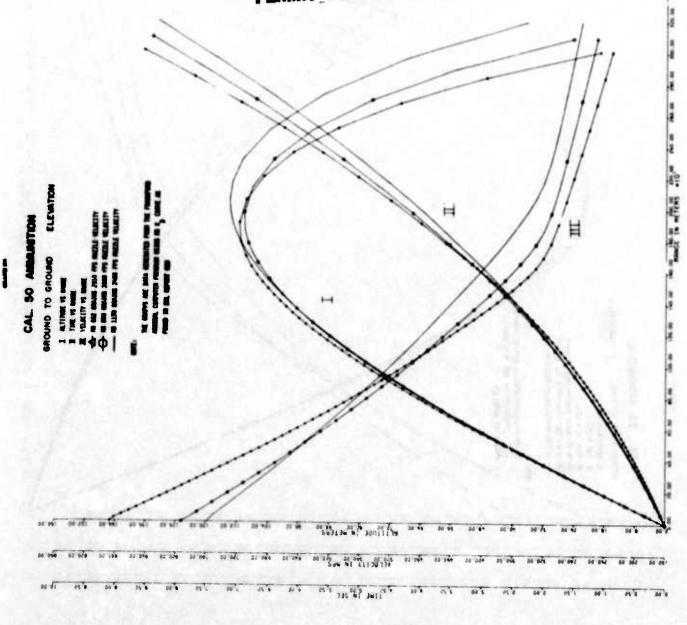


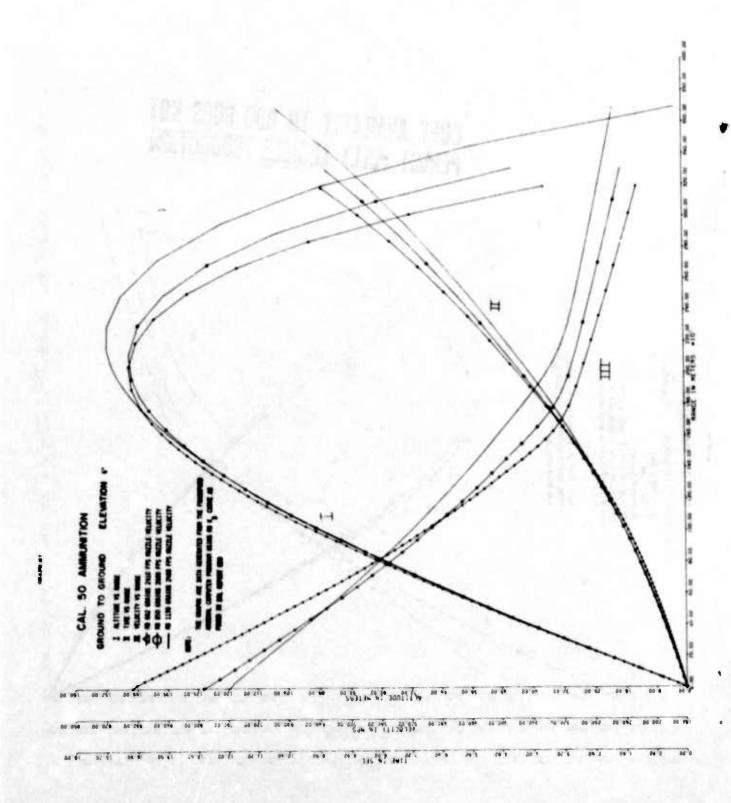


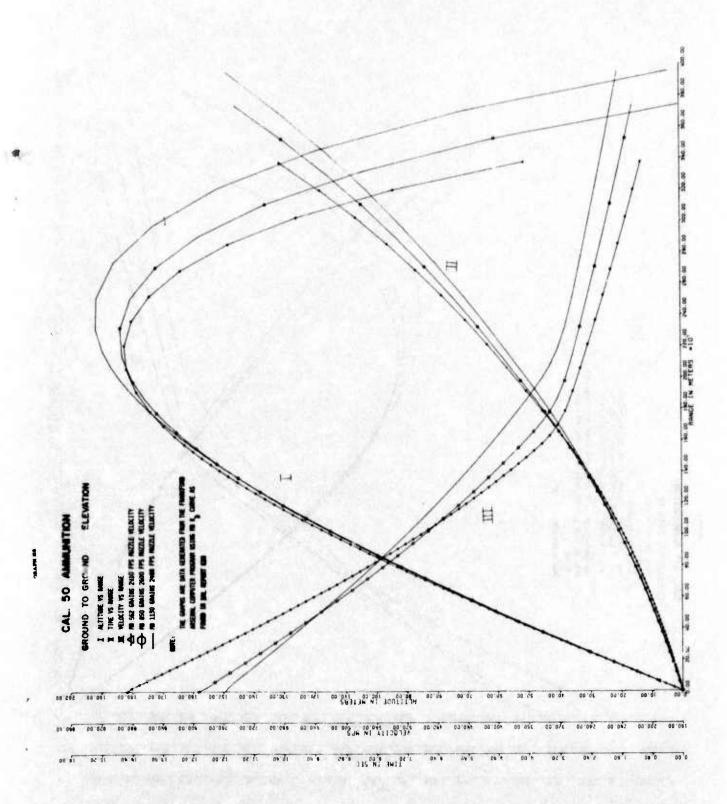
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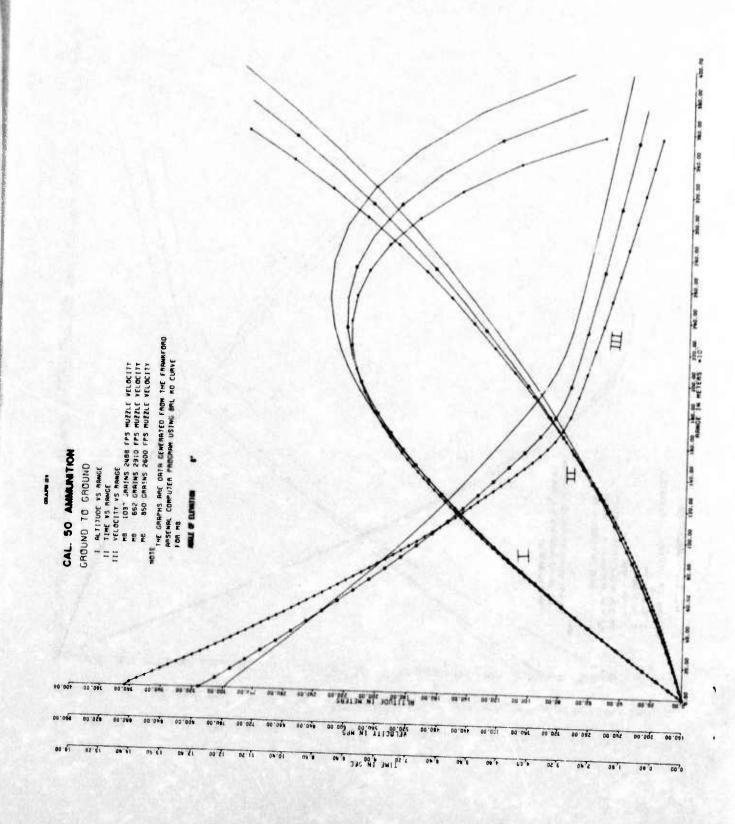


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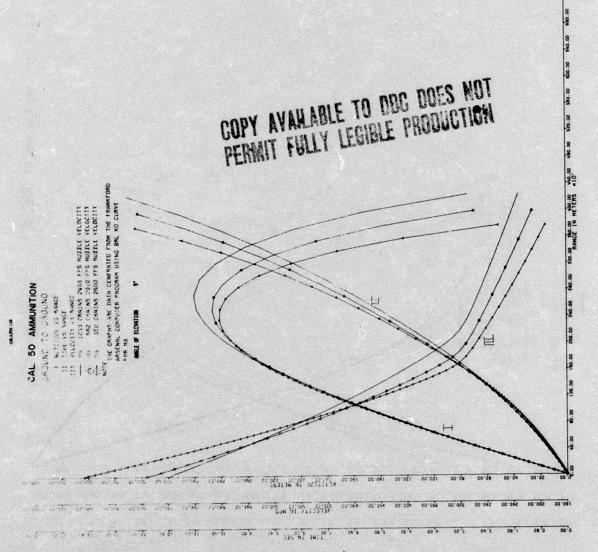


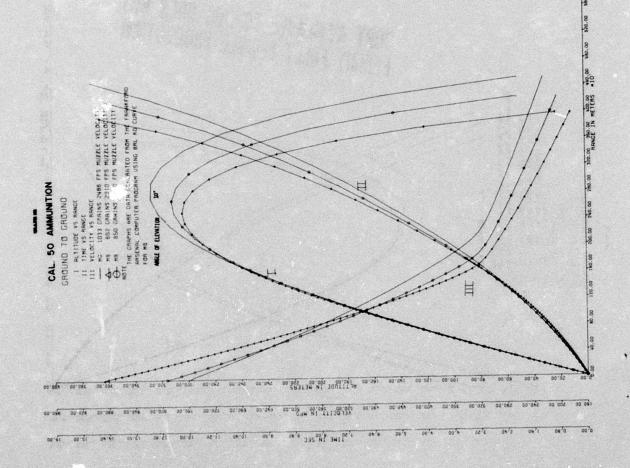


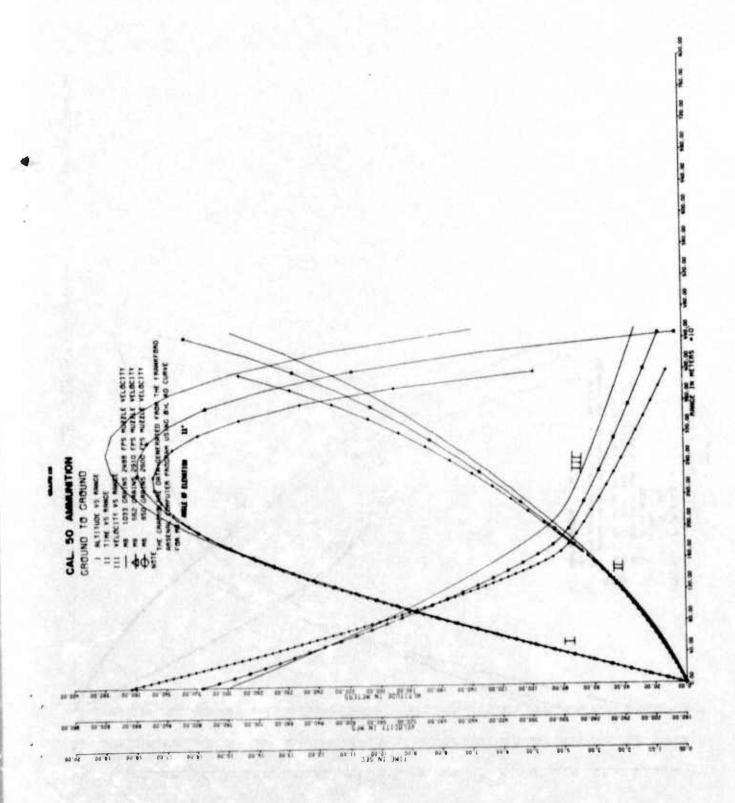


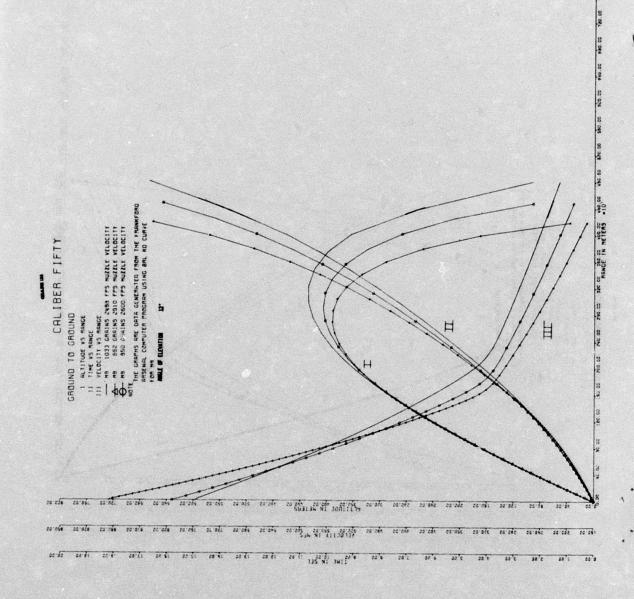


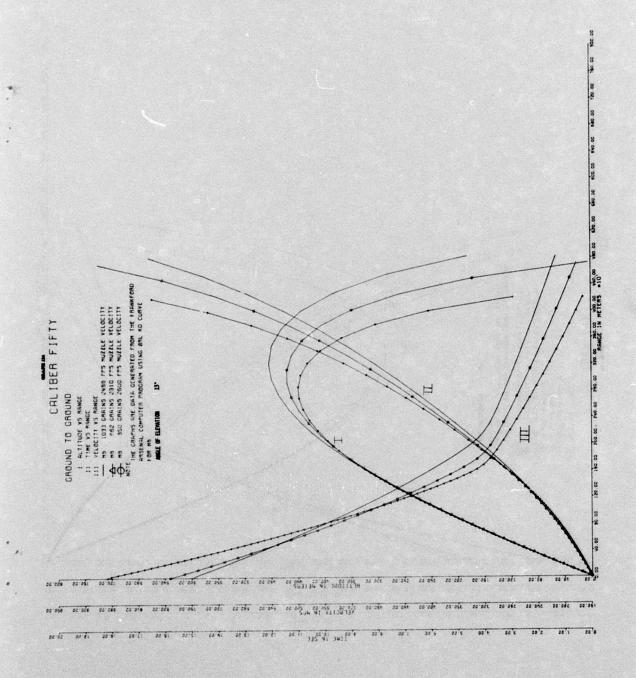
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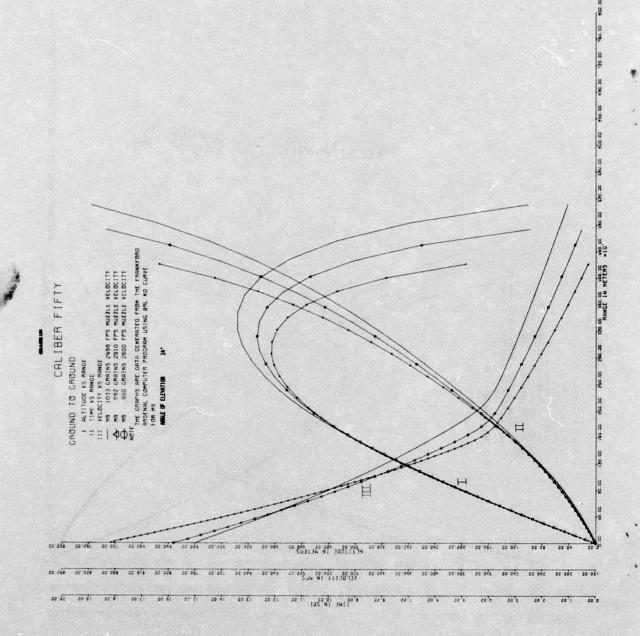


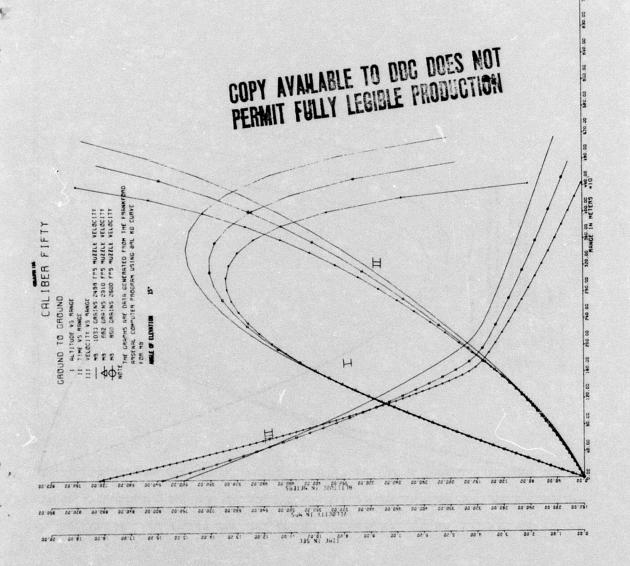


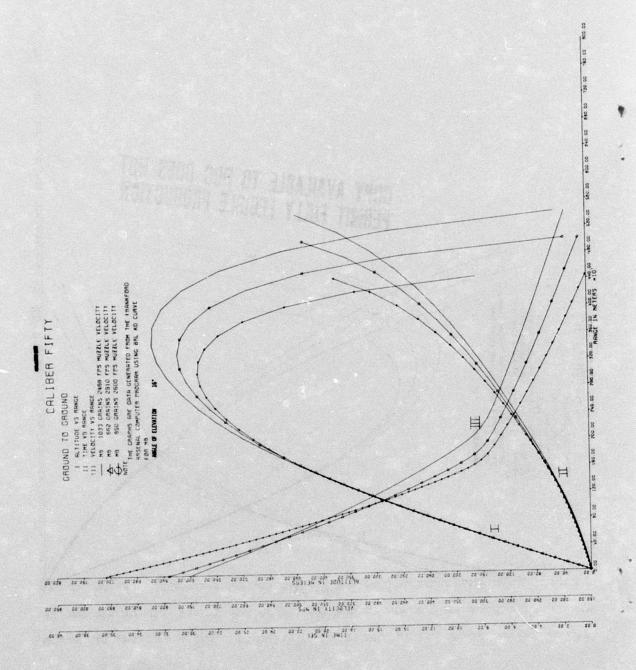


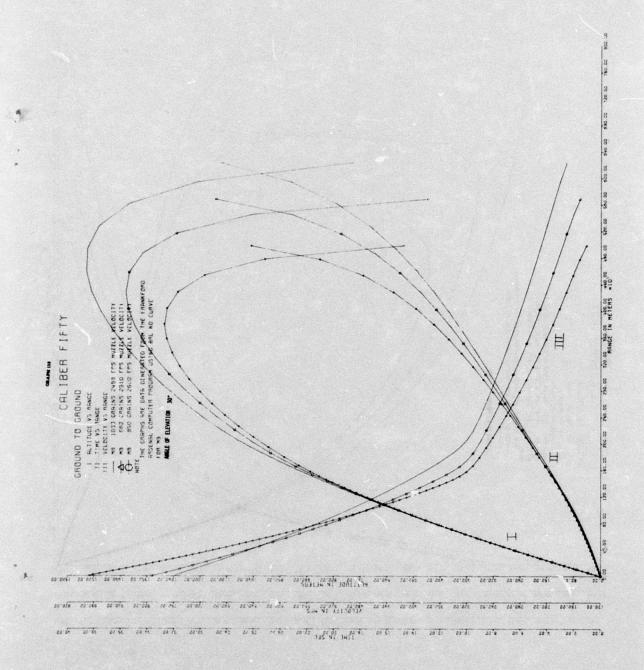


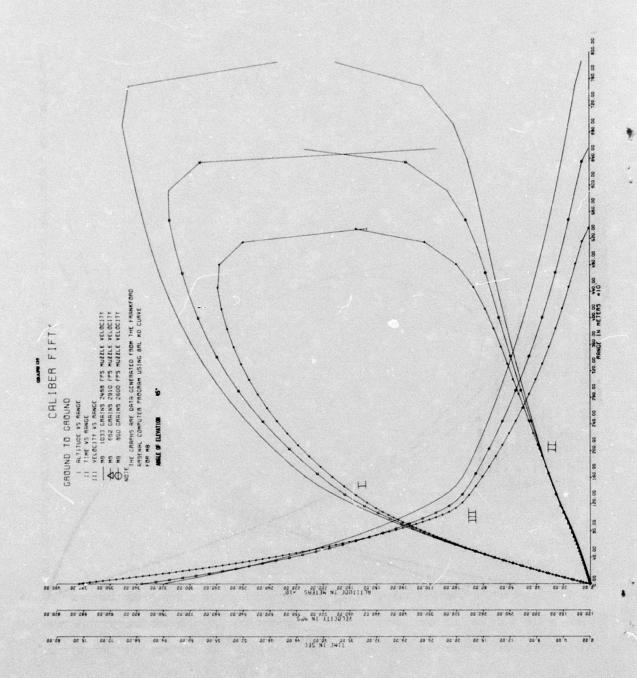


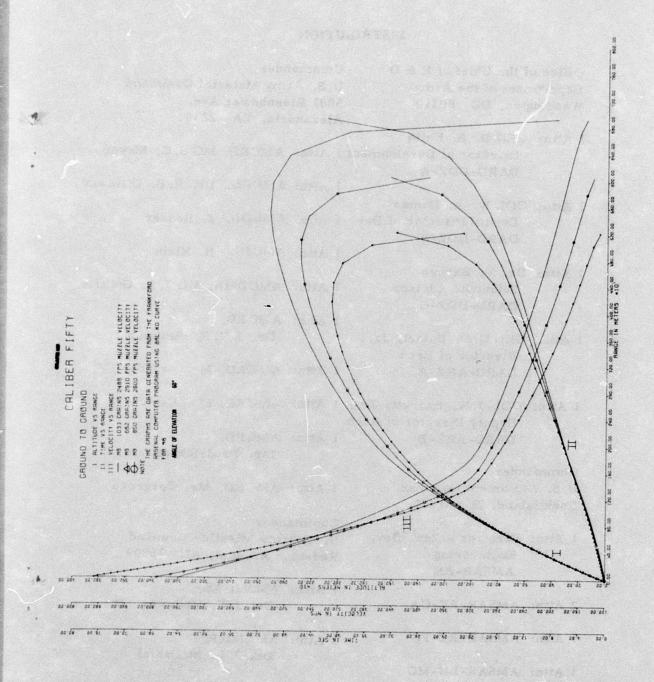












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